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CINCINNATI UNIV OH DEPT OF ENGINEERING SCIENCE  
A CRITICAL EVALUATION OF COMPUTER SUBROUTINES FOR SOLVING STIFF--ETC(U)  
OCT 78 D C KRINKE, R L HUSTON  
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A CRITICAL EVALUATION OF  
COMPUTER SUBROUTINES FOR  
SOLVING STIFF DIFFERENTIAL EQUATIONS

Dennis C. Krinke  
and  
Ronald L. Huston

15 Oct 78

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## I. INTRODUCTION

The integration of initial valued simultaneous differential equations commonly occurring in models of large, complex mechanical systems (for example, human body/crash victim models, finite-segment structural system models, and large vibrating system models) has been shown to be costly in both CPU time and "turn-around" time. Indeed, developers of such models have found the efficiency of the differential equation integrators to be the most critical aspect of a model's overall efficiency [1,2,3]. Hence the search for efficient integrating subroutines or "solvers" has been long standing and is continuing.

Shampine, Watts, and Davenport [4] have made an extensive evaluation of computer codes for "nonstiff" differential equations. They suggest, however, that there are special problems which arise in the solution of "stiff" differential equations.<sup>1</sup> It has been observed by Huston and Hessel [5] that the differential equations of large mechanical system models are frequently stiff. Hence, there is both academic as well as utilitarian interest in a critical, comparative evaluation of the commonly used and commonly available solvers as applied to stiff equations.

Solution time and accuracy are the primary concerns when solving the differential equations of large mechanical system models. Hence,

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<sup>1</sup>The following section of the report contains a definition of "stiffness" as associated with differential equations.



it was decided to test the available solvers on equation's where exact analytical solutions were available. However, the derivative functions (that is, "the right-hand side") of the equation for system models are generally significantly more complex than the corresponding functions for test equations for which exact solutions are known. Consequently, the subroutine which evaluates the derivative functions for system models consumes considerably more CPU time. Therefore, a measure of the efficiency of a differential equation solver is the number of function calls it needs to make to the derivative evaluating subroutine to integrate the equations while holding a given accuracy. Indeed, this is probably a better measure of the potential efficiency of a solver than the actual CPU time used to solve test equations. Thus, in the test cases considered herein, both CPU time and number of function calls are used for comparison of the solvers.<sup>1</sup>

The balance of this report is divided into six sections with the next section providing definitions of "stiffness". This is followed in the next three sections by a description of the subroutines tested, the test systems, and the test procedures. The final two sections contain the results and conclusions of the tests. Recommendations for further study are presented in the final section. Finally, an outline of the analytical solution of one of the test systems, together with a listing of the subroutines of the solvers tested are given in the Appendices.

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<sup>1</sup>On one occasion, a program was run twice without modification and even though all other results were exactly the same, the CPU times differed by 6%. Apparently the time measurement is not as reproducible as other computer operations. Therefore when comparing these values, it is suggested that one should not expect them to be more than 5% accurate.

## II. DEFINITION OF STIFFNESS

Two definitions of "stiffness" appear in literature. One defines a "stiff" linear system of differential equations as one which has widely separated eigenvalues or time constants [6,7,8,9,10]. The other associates "stiffness" with the presence of diverging exponential terms which exist in the general solution but happen to have zero coefficients in the actual solution due to the particular choice of initial conditions [11,12,13]. It is not clear that these definitions are equivalent; hence, systems which are best described by the first definition will be said to have "Type 1 stiffness" and systems which are best described by the second will be said to have "Type 2 stiffness".

Systems with Type 1 stiffness are expensive to integrate since a transient portion of the solution, which has long since decayed, prevents an increase in stepsize even though the solution at that point may be quite smooth [10,9].

Systems with Type 2 stiffness are difficult to integrate because algorithm approximation, roundoff and truncation error introduce non-zero coefficient values to the divergent exponential terms. Although these coefficients may be small, the exponential term can still grow to be large in the interval of integration [11,13]. This can, in turn, greatly reduce the accuracy of the solution.

### III. SOLVER SUBROUTINE DESCRIPTIONS

Table 1. summarizes the subroutines tested and the numerical methods of each. The only subroutines tested were those that were believed to be generally available.

All of the subroutines are written in FORTRAN and are compatible with the AMDAHL 470 in use at the University of Cincinnati. DRKGS and DHPCG are interval oriented, while DVOGER, DREBS, and RK45 are step oriented. RK45 uses a constant stepsize, but all of the others use automatic stepsize adjustment. All of the routines were coded in double precision.<sup>1</sup>

Subroutine Name	Source	Method
DRKGS	[14]	Fourth Order Runge-Kutta
DHPCG	[14]	Hamming Predictor-Corrector
DVOGER(ADAMS)	[15]	Adams Predictor-Corrector
DVOGER(GEAR)	[15]	Gear Predictor-Corrector
DREBS	[15]	Modification of Bulirsch-Stoer ALGOL Routine DESUB
RK45	[16]	Sixth Order Runge-Kutta

Table 1. Solver Subroutine Summary

DRKGS uses a fourth order Runge-Kutta method (as modified by Gill) [14]. Some pertinent characteristics of DRKGS are as follows:

---

<sup>1</sup> RK45 was obtained in single precision, but was modified to use double precision for the test runs.

- (1) Local error estimation is accomplished by comparing the solution computed in two steps of stepsize  $h$  to the solution obtained in one step of stepsize  $2h$ ;
  - (2) Separate error tolerances are required for each function in the system;
  - (3) The maximum stepsize is also used for the initial stepsize and the minimum stepsize is  $2^{-10}$  of this value<sup>1</sup>;
- and (4) An output subroutine which is called after every step is required and is expected to perform all output duties.

DHPCG and DRKGS have been written to be easily interchanged. (The parameter lists are all identical.) To change from one subroutine to the other requires only a change in the dimension of a work array. However, DHPCG uses a completely different algorithm, that is, a Hamming predictor-corrector method [14], with a fourth order Runge-Kutta technique is used to generate the starting values. Once again, local error estimation is accomplished by comparing the solution obtained in one step of stepsize  $h$  to that obtained in two steps of stepsize  $h/2$  and the same limitations on minimum, initial, and maximum stepsize which exist for DRKGS, exist for DHPCG.

DVOGER [15] is a modification of the subroutine DIFSUB written by C.W. Gear [17]. This routine contains two methods:

---

<sup>1</sup>For one of the tests, it was necessary to modify this in order to obtain a solution.



- (1) An Adam's predictor-corrector method of variable order and stepsize which is intended for use with nonstiff systems;
- and (2) Gear's modification of the Adam's method which is intended for use with stiff systems [18].

The pertinent characteristics of DVOGER are:

- (1) Gear's method seeks to have not only the usual derivatives, but also the gradient of these functions. However, if it is not convenient to supply coding to evaluate this gradient, an option is provided that numerically approximates the gradient when given only the standard derivatives;
- (2) Only a single error tolerance is permitted which is applied to all functions;
- (3) Separate specifications of minimum, initial, and maximum stepsize are permitted;
- and (4) Since DVOGER computes only a single step at each call, the user has the flexibility of utilizing either absolute or relative error control.

DREBS [15] is a modification of the Bulirsch-Stoer ALGOL routine DESUB. Like DVOGER, DREBS permits only one error tolerance which is applied to all functions and both absolute and relative error specifications are possible. However, although minimum and initial stepsizes may be specified, a maximum stepsize cannot be specified.

RK45 [16] computes both a fourth and a fifth order Runge-Kutta approximation to the solution at every step and then uses Richardson's



method to achieve sixth order accuracy.<sup>1</sup> RK45 does not estimate the local error or adjust stepsize. Furthermore, the derivative evaluating subroutine must be named XKOTEQ (although this would be simple to modify if it were inconvenient). RK45 is step oriented; however, without error control, this is no more flexible than interval orientation would be.

---

<sup>1</sup>The coefficients of the Runge-Kutta formulae have been optimized for maximum numerical stability.

#### IV. TEST SYSTEMS

Five systems of stiff differential equations were chosen to evaluate the solvers. As much as possible, systems were chosen in which the stiffness could be varied and the trend in solver efficiency observed. Systems 1, 2, and 3 contain Type 1 stiffness and systems 4 and 5 contain Type 2.

System 1 is presented in Reference [6] and represents a very simple system of differential equations that contain Type 1 stiffness. The system is:

$$\dot{\underline{y}} = [A] \underline{y} \quad (1)$$

where

$$[A] = \begin{bmatrix} -a & b \\ b & -a \end{bmatrix} \quad (2)$$

and

$$\underline{y}(0) = \begin{bmatrix} 0 \\ 2 \end{bmatrix} \quad (3)$$

An analytical solution is:

$$\underline{y}(t) = \begin{bmatrix} e^{-\alpha_1 t} & - e^{-\alpha_2 t} \\ e^{-\alpha_1 t} & + e^{-\alpha_2 t} \end{bmatrix} \quad (4)$$

where  $\alpha_1 (= a-b)$ ,  $\alpha_2 (= a+b)$  are the eigenvalues of A. If  $\alpha_1$  and  $\alpha_2$  are nearly equal, then the system is nonstiff, but if  $\alpha_1$  and  $\alpha_2$  have widely separated values, the system is stiff.<sup>1</sup> The test was conducted with the parameters shown in Table 2 and Figure 1 illustrates the solution with  $\alpha_1 = 1$  and  $\alpha_2 = 5$ .

$\alpha_1$	$\alpha_2$	a	b	Period of Integration
1	2	1.5	0.5	5
1	5	3.0	2.0	5
1	10	5.5	4.5	5
1	20	10.5	9.5	5
1	50	25.5	24.5	5
1	100	50.5	49.5	5
1	200	100.5	99.5	5
1	500	200.5	249.5	5
1	1000	500.5	449.5	5

Table 2. System 1 Test Parameters.

<sup>1</sup>Interestingly, in this simple system, one can perform the transformation:

$$\underline{\omega} = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 & 1 \\ 1 & -1 \end{bmatrix} \underline{y}$$

which couples the equations. That is, in terms of  $\underline{\omega}$ , the system

$$\text{becomes: } \dot{\underline{\omega}} = \begin{bmatrix} -\alpha_1 & 0 \\ 0 & -\alpha_2 \end{bmatrix} \underline{\omega}.$$

With the equations decoupled, they can be solved separately and the stiffness is removed from the system,

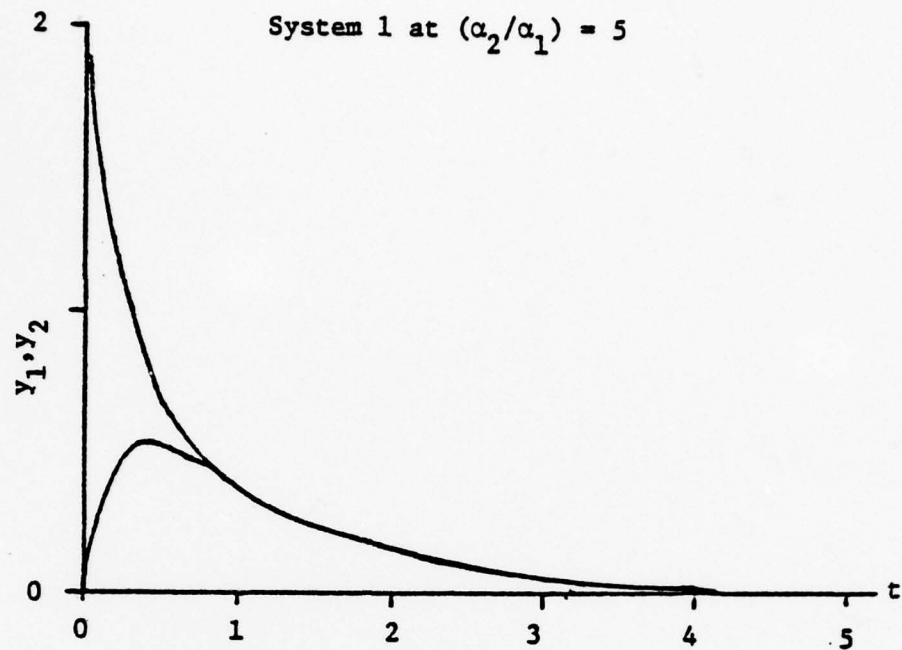


Figure 1. System 1 Exact Solution.

System 2 consists of the double mass-damper-spring system shown in Figure 2. Its governing equations are:

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \ddot{\underline{y}} + \begin{bmatrix} c_1+c_2 & -c_2 \\ -c_2 & c_2 \end{bmatrix} \dot{\underline{y}} + \begin{bmatrix} k_1+k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \underline{y} = \underline{0} \quad (5)$$

Let the initial conditions be:

$$\underline{y}(0) = \begin{bmatrix} 1 \\ 1+k_1/k_2 \end{bmatrix} \quad (6)$$

$$\dot{\underline{y}}(0) = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \quad (7)$$

When the system is underdamped, the analytical solution<sup>1</sup> has the form:

$$y_1(t) = A_1 e^{-\alpha_1 t} \cos(\omega_1 t + \phi_1) + A_2 e^{-\alpha_2 t} \cos(\omega_2 t + \phi_2) \quad (8a)$$

and

$$y_2(t) = A_3 e^{-\alpha_1 t} \cos(\omega_1 t + \phi_3) + A_4 e^{-\alpha_2 t} \cos(\omega_2 t + \phi_4) \quad (8b)$$

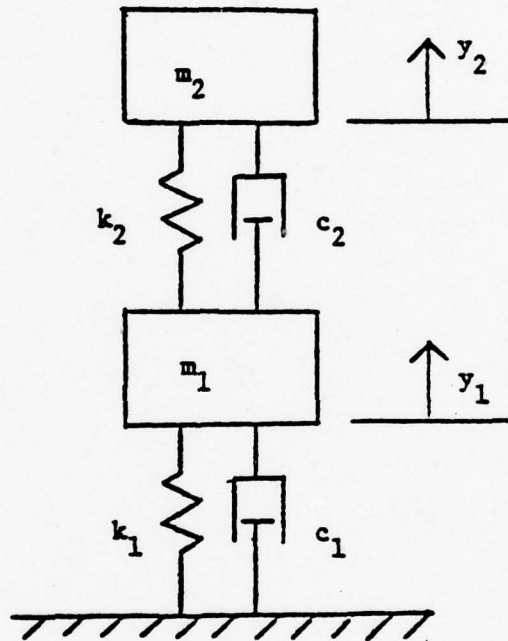


Figure 2. System 2. Model.

This solution contains damped exponential terms with time constants  $\alpha_1$  and  $\alpha_2$ . Hence, the problem is nonstiff if  $\alpha_1$  and  $\alpha_2$  are nearly equal, but has Type 1 stiffness if they have widely separated values. The system parameters  $m_1$ ,  $m_2$ ,  $c_1$ ,  $c_2$ ,  $k_1$ , and  $k_2$  were chosen to obtain the desired values of  $\alpha_1$ ,  $\alpha_2$ ,  $\omega_1$ , and  $\omega_2$ . The test was conducted with

<sup>1</sup>The analytical solution to this system is derived in Appendix A.



the parameters shown in Table 3 and Figure 3 illustrates the solution with  $\alpha_1 = 1$  and  $\alpha_2 = 5$ .

$\alpha_1$	$\alpha_2$	$\omega_1$	$\omega_2$	Period of Integration
1	2	$2\pi$	$6\pi$	5
1	5	$2\pi$	$6\pi$	5
1	10	$2\pi$	$6\pi$	5
1	20	$2\pi$	$6\pi$	5
1	50	$2\pi$	$6\pi$	5
1	100	$2\pi$	$6\pi$	5
1	200	$2\pi$	$6\pi$	5
1	500	$2\pi$	$6\pi$	5
1	1000	$2\pi$	$6\pi$	5

TABLE 3. System 2 Test Parameters.

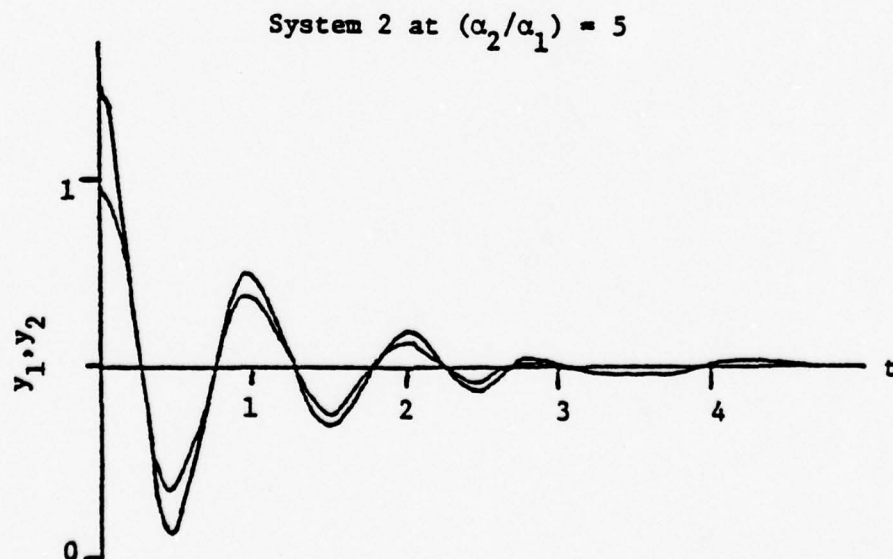


Figure 3. System 2 Exact Solution.

System 3 was obtained from References [6,17] and is attributed to F. T. Krogh. The equation

$$\dot{y} = -\beta y + y^2 \quad \text{with } y(0) = -1 \quad (9)$$

has the analytical solution:

$$y(t) = \frac{\beta}{1 - (1 + \beta)e^{\beta t}} \quad (10)$$

If one takes the system of four uncoupled equations:

$$\dot{y}_i = -\beta_i y_i + y_i^2, \quad (11)$$

$$y_i(0) = -1, \quad i = 1, 2, 3, 4 \quad (12)$$

and performs the transformation:

$$\underline{y} = [U] \underline{y} \quad (13)$$

where

$$[U] = \frac{1}{2} \begin{bmatrix} -1 & 1 & 1 & 1 \\ 1 & -1 & 1 & 1 \\ 1 & 1 & -1 & 1 \\ 1 & 1 & 1 & -1 \end{bmatrix} \quad (14)$$

then the system becomes

$$\dot{\underline{w}} = -[U] [B] [U] \underline{w} + [u] \underline{z} \quad (15)$$

$$\text{with } w_i(0) = -1 \quad i = 1, 2, 3, 4 \quad (16)$$

$$\text{where } [B] = \begin{bmatrix} \beta_1 & 0 & 0 & 0 \\ 0 & \beta_2 & 0 & 0 \\ 0 & 0 & \beta_3 & 0 \\ 0 & 0 & 0 & \beta_4 \end{bmatrix} \quad (17)$$

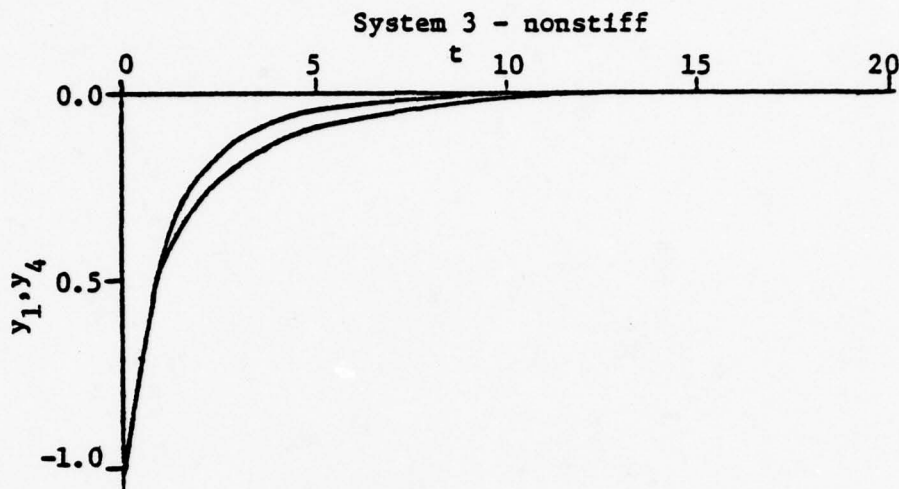
$$\text{and } z_i = w_i^2 \quad (18)$$

In this form, the equations are coupled and have Type 1 stiffness. Krogh suggests letting the values for the  $\beta_i$ 's be 0.1, 0.2, 0.3, and 0.4 for a nonstiff problem and 1000, 800, -10, and 0.001 for a stiff problem. The test was conducted with both sets of these values and Figure 4 illustrates the nonstiff solution. The period of integration was 20 for the nonstiff problem and was 1000 for the stiff problem.

System 4 is presented in Reference [11] and consists of the single equation:

$$\dot{y} = 5(y - t^2) \quad t \in (0, 5) . \quad (19)$$

The general analytical solution is:



$$y(t) = C e^{5t} + t^2 + 0.4t + 0.08 \quad . \quad (20)$$

In the special cases where  $y(0) = 0.08$ , the value of  $C$  is exactly zero. However, algorithm approximation, roundoff and truncation errors cause the numerical solution to contain a  $ke^{5t}$  term.  $k$  must be very small indeed for  $ke^{5t}$  to be small in comparison to the exact solution, which is shown in Figure 5.

System 5 was a clear example of Type 2 stiffness but it lacked a means of varying that stiffness. System 5 does not obviously have Type 2 stiffness, but it behaves in sufficiently similar manner to suggest that it does.

System 5 models a central force orbit (two body problem with the mass of one body much larger than the other). Elliptical orbits

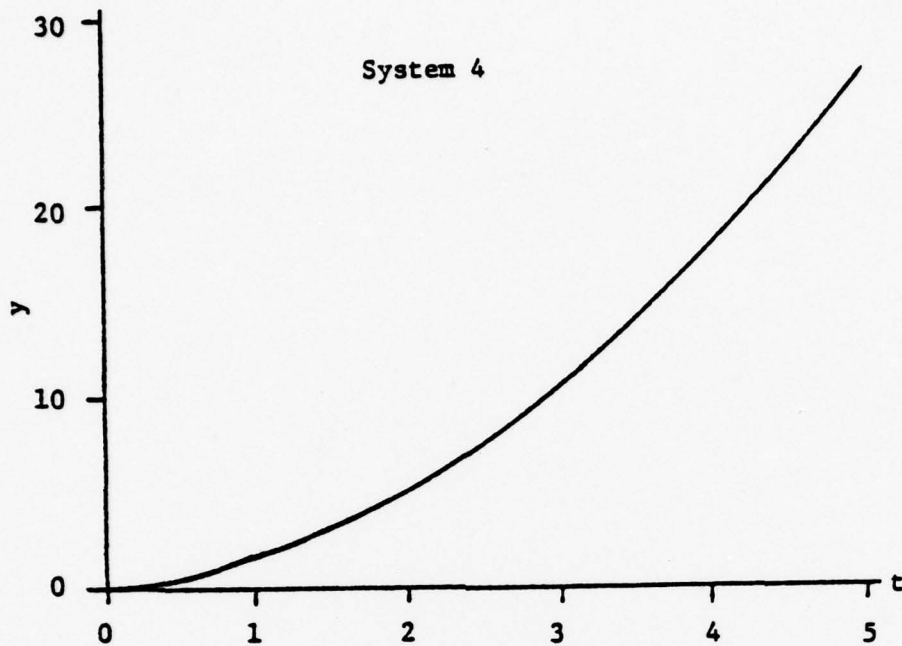


Figure 5. System 4 Exact Solution.

were chosen so that they would be periodic. The eccentricity of the ellipse was varied from moderately elliptical to highly "cigar-shaped" in order to change the amount of stiffness. The governing equations for this system are:

$$\ddot{r} = r\dot{\theta}^2 - \frac{GM}{r^2} \quad (21a)$$

$$\ddot{\theta} = -2\dot{r}\dot{\theta}/r \quad (21b)$$

where  $G$  and  $M$  are constants.

The initial conditions (which correspond to the apogee) are:

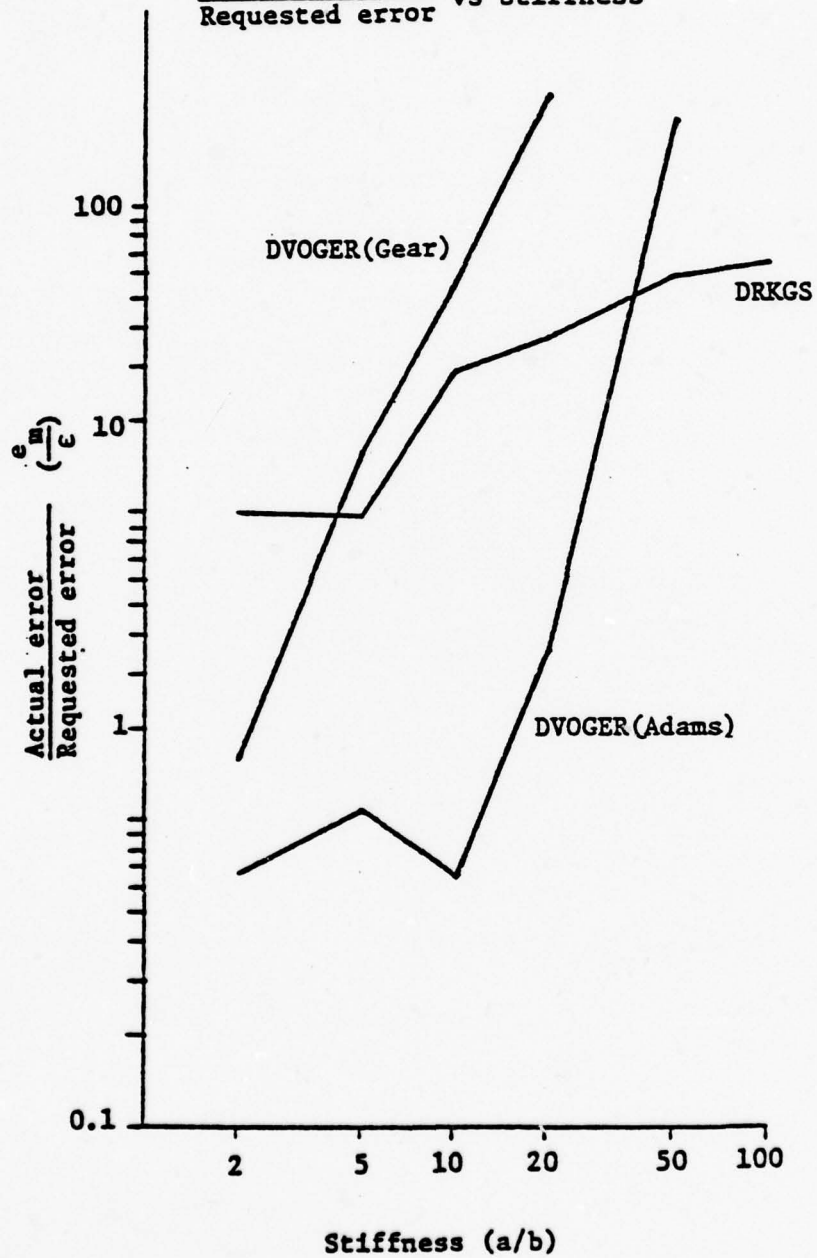
$$r(0) = a(1+e) \quad (22a)$$

$$\theta(0) = -\pi \quad (22b)$$



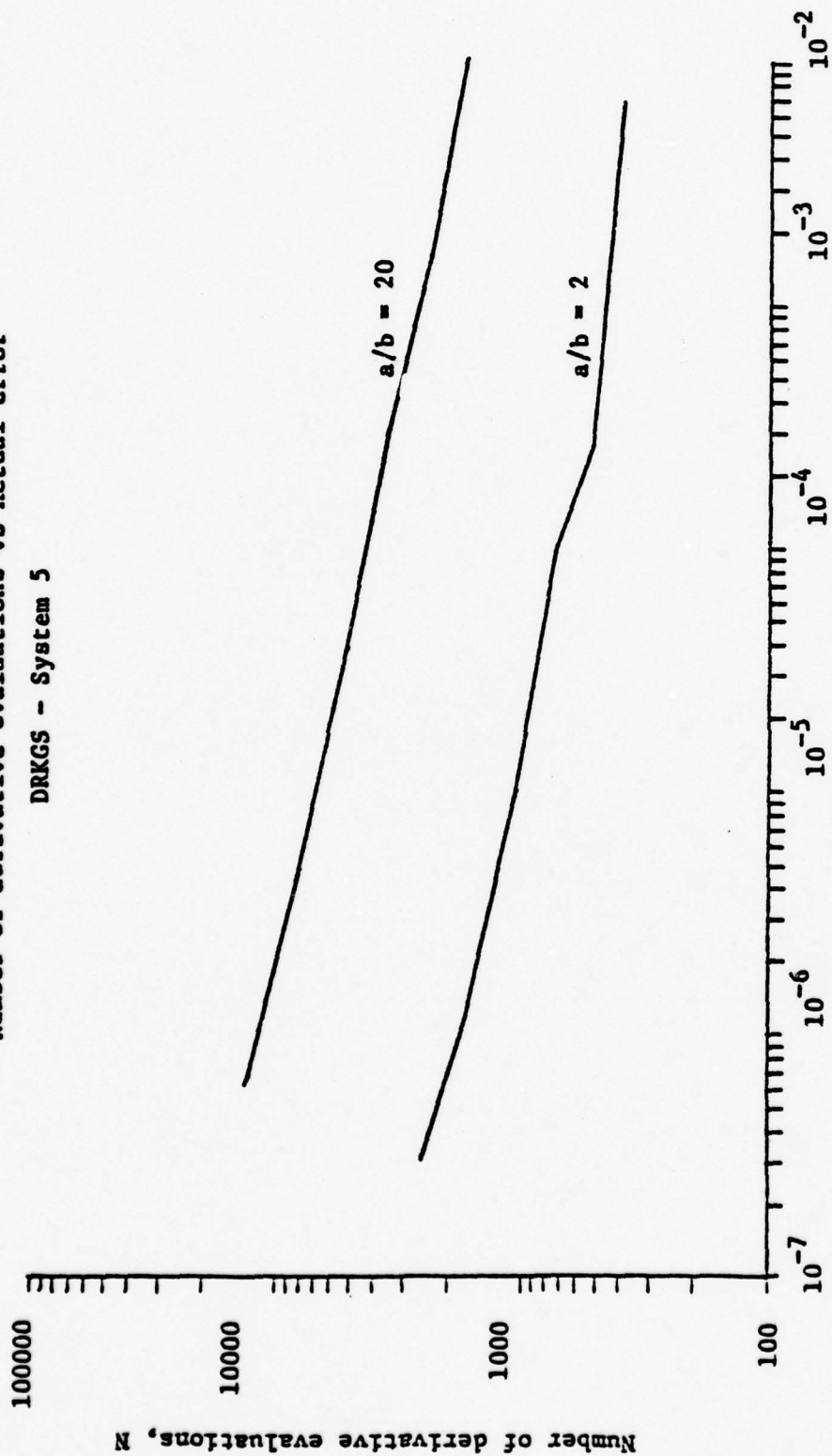
# System 5

Actual error  
Requested error vs Stiffness



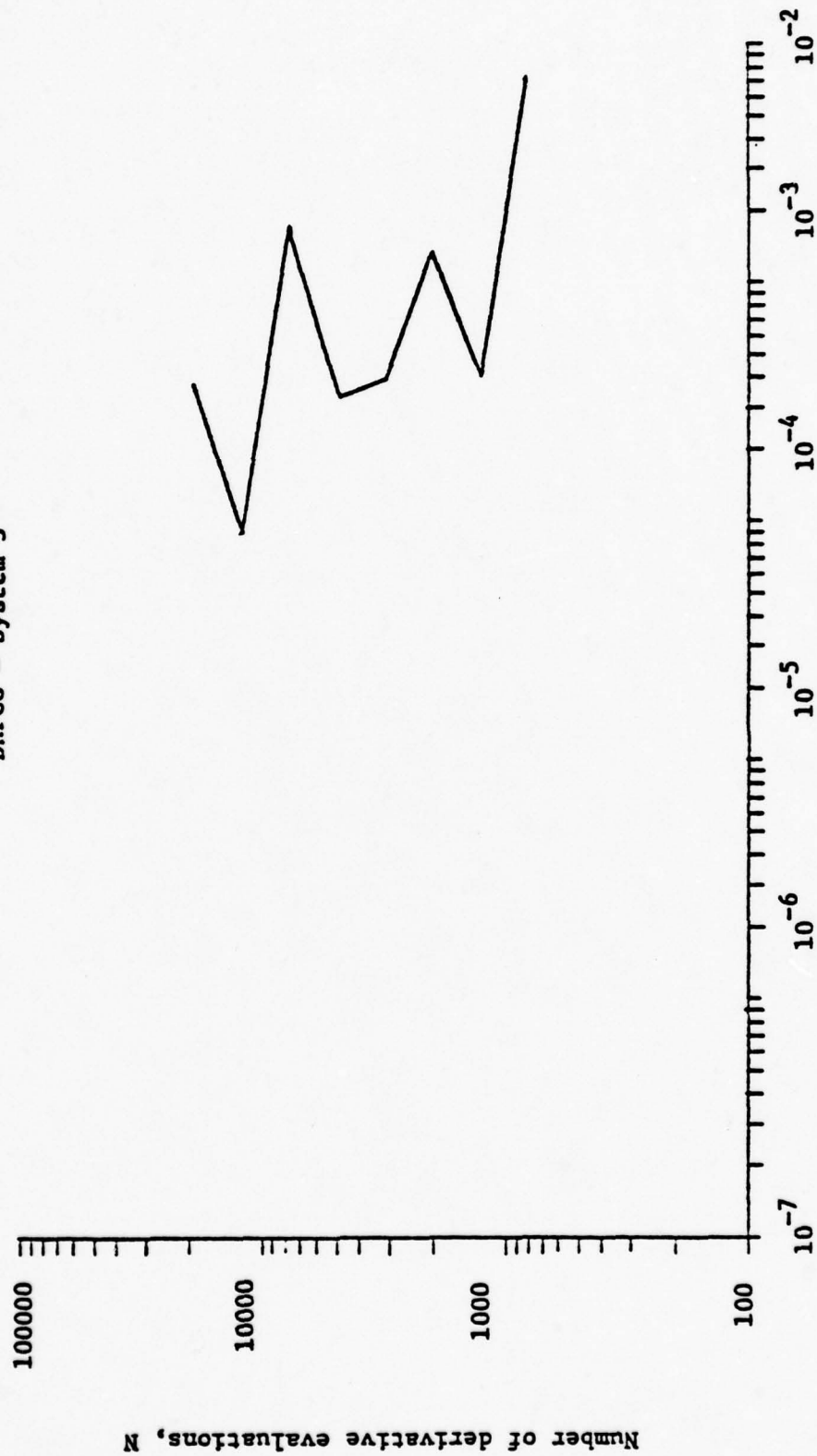
Graph 5. Accuracy vs. Stiffness - System 5.

Number of derivative evaluations vs Actual error  
DRKGS - System 5

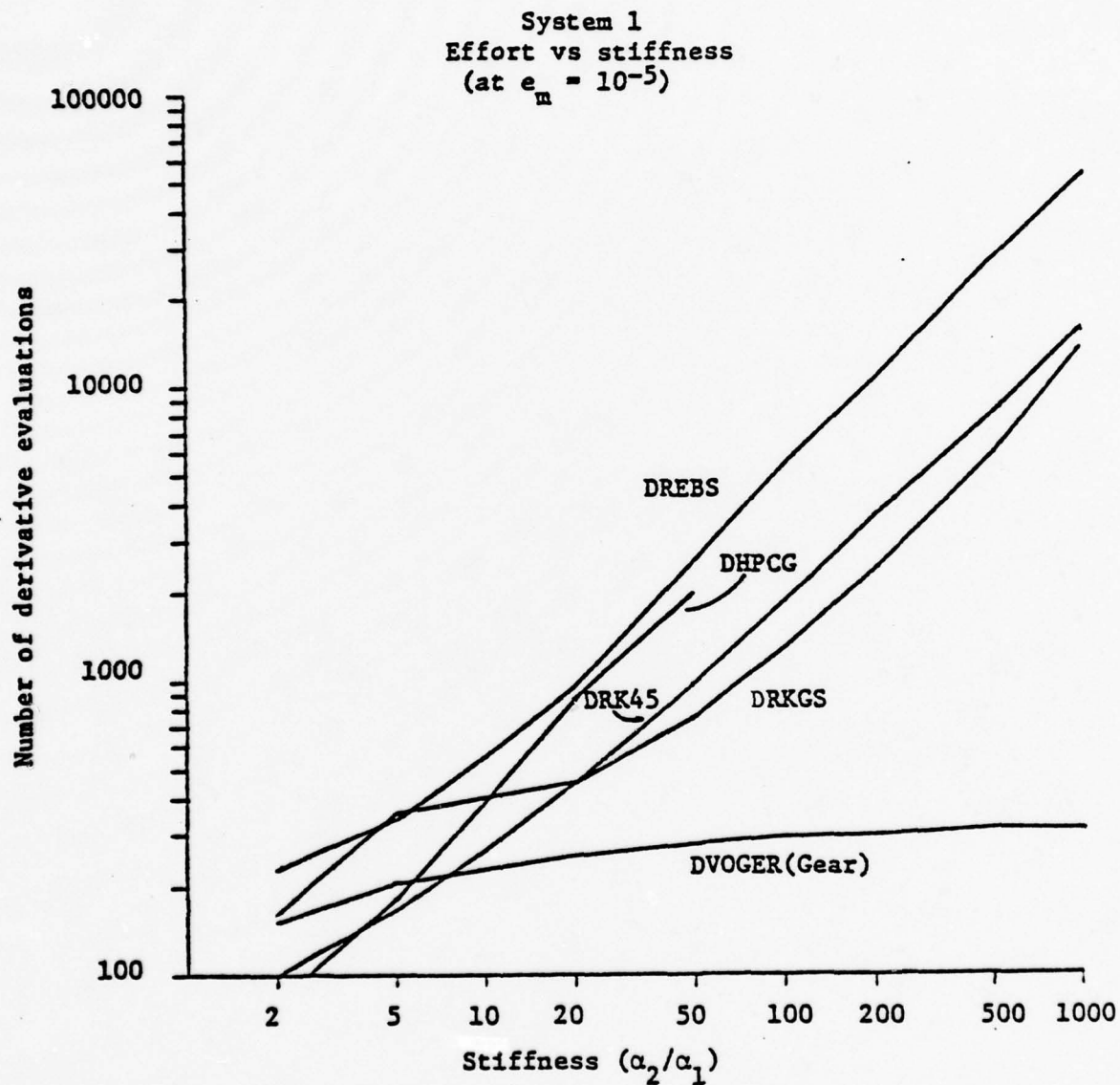


Graph 6. Effort vs. Accuracy - System 5 - DRKGS

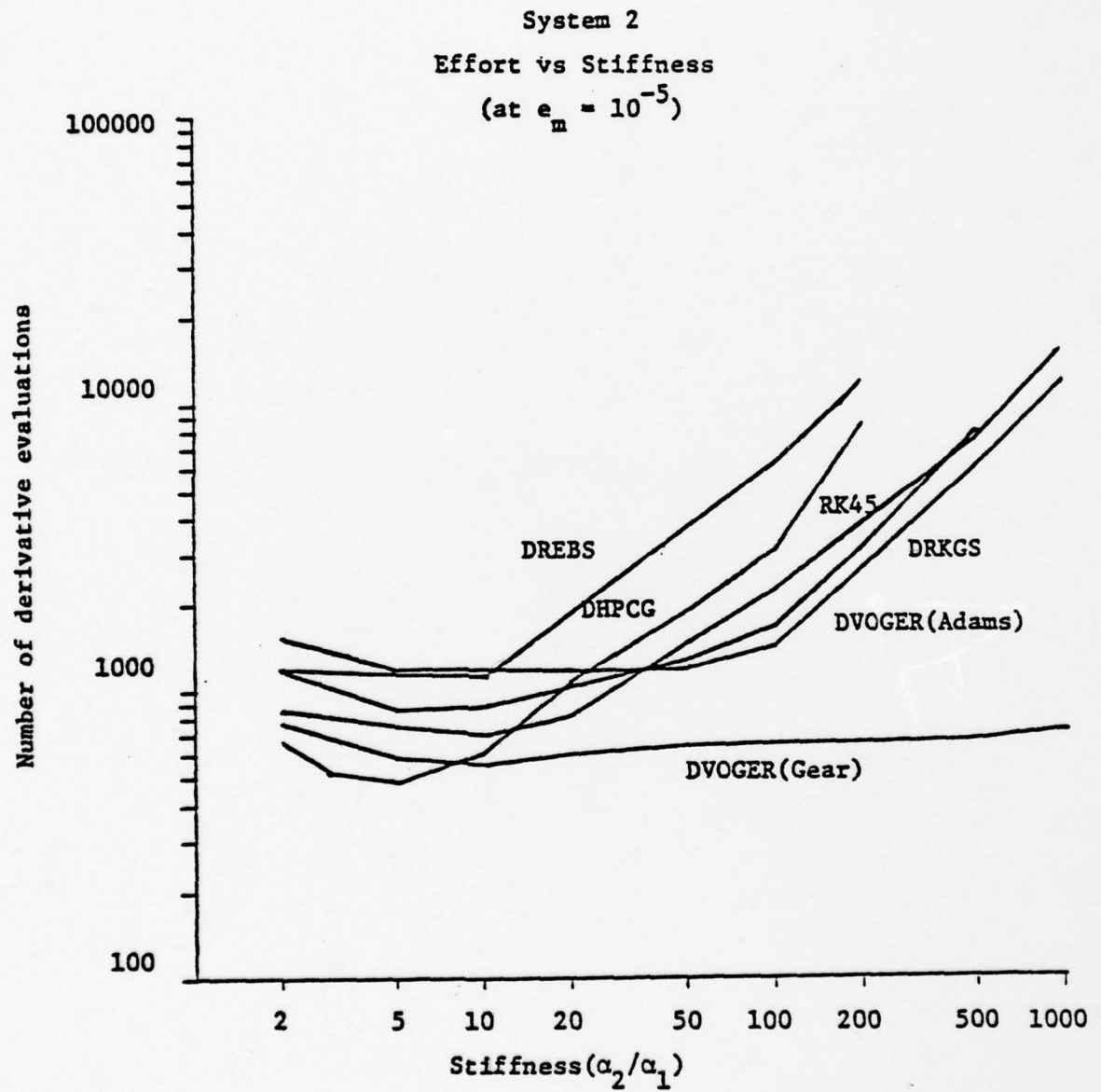
Number of derivative evaluations vs Actual error  
 DHPGG - System 5



Graph 7. Effort vs. Accuracy - System 5 - EHPGG

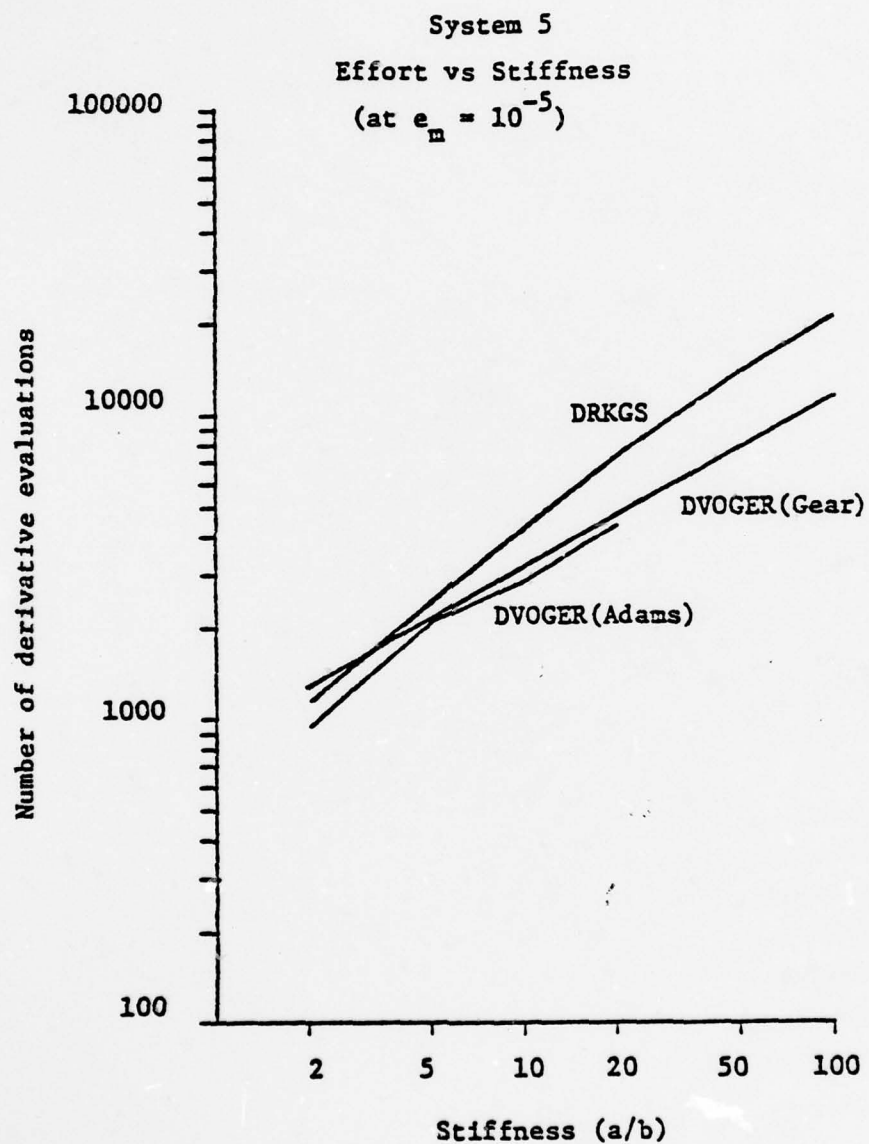


Graph 8. Effort vs. Stiffness - System 1.

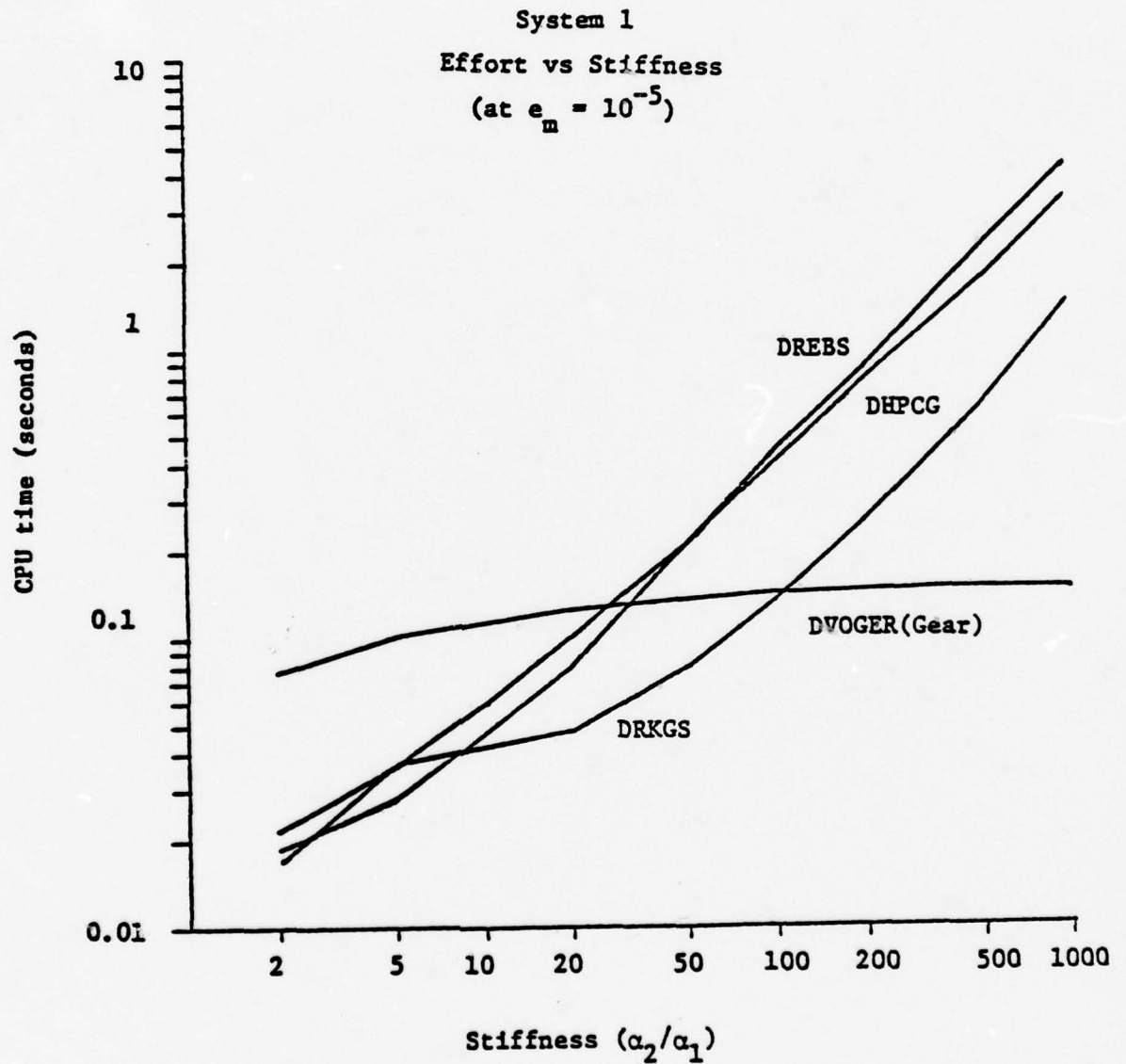


Graph 9. Effort vs. Stiffness - System 2.





Graph 10. Effort vs. Stiffness - System 5.



Graph 11. CPU Time vs. Stiffness - System 1.

## VII. CONCLUSIONS AND RECOMMENDATIONS

Two significant and important conclusions can be drawn from this research effort. First, the solvers may not yield the requested accuracy when integrating a system with Type 2 stiffness. This suggests that the integration of such systems is not automatic at all. Rather, one must integrate every such system at least twice with different requested error tolerances ( $\epsilon$ ) and compare solutions. While such stiff systems are not as common as non-stiff systems, the user should be cautioned that they do exist.

Secondly, if a system has Type 1 stiffness and if the derivative evaluations are expensive, a routine using Gear's method (such as DVOGER) should be used. Gear's method was designed especially for stiff systems and it can be strikingly more efficient than the other solver routines.

Beyond this, experience with these subroutines prompts a few other remarks and opinions: First, even in system that were not stiff, the actual maximum error ( $e_m$ ) frequently differed from that requested ( $\epsilon$ ) by factors of 20 or more. The subroutines would be more satisfying if their global error estimation could be improved.

Secondly, RK45 does not have automatic stepsize capability and was difficult to use. This emphasized the convenience of the automatic stepsize adjustment of the other subroutines. Even if one must solve every problem twice with them it is much better than making four or five runs to find the correct stepsize for RK45.<sup>1</sup>

---

<sup>1</sup>When the stepsize is too large for RK45, numerical instability occurs, leading to exponential overflow.

Third, the interval oriented format of DRKGS and DHPCG was convenient. Also, placing all of the output duties into a subroutine gives a modular property to the coding and further simplifies their use. However, the inability to separately specify the initial and maximum value of stepsize in these routines is disastrous to efficiency when looking for long time solutions in systems with decaying transients. Also, it is sometimes necessary to extend the permitted number of stepsize bisections to obtain solutions. Ten bisections may be a reasonable limit for single precision work, but forty or even fifty can be required for double precision integrations.

Finally, DVOGER and DREBS have no provision for the specification of separate error tolerances for the different functions in the system. While this presented no serious difficulty for this work, it could conceivably be important for a system with functions of greatly different magnitudes. The step oriented format of DVOGER and DREBS does however possess the potential for greater flexibility, particularly in error control. For example, if one suspected Type 2 stiffness, an exponential distribution of error per step would probably be better than a linear distribution.

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$$\dot{r}(0) = 0 \quad (22c)$$

$$\dot{\theta}(0) = 2\pi ab / (r^2(0)T) \quad (22d)$$

where  $a$  and  $b$  are respectively the major and minor semi-axes of the ellipse,  $e$  is the eccentricity ( $\sqrt{1-(b/a)^2}$ ), and  $T$  is the period of the orbit. To achieve a period  $T$ , it is necessary to set  $GM = a^3(2\pi/T)^2$ . The exact solution is simple only at  $t = T$ :

$$r(T) = r(0) \quad (23a)$$

$$\theta(T) = \pi \quad (24b)$$

The test was conducted with the parameters given in Table 4 and Figure 6 illustrates the solution for  $a/b = 2$ .

$a$	$a/b$	$T$
5	2	1
5	5	1
5	10	1
5	20	1
5	50	1
5	100	1

TABLE 4. System 5 Test Parameters.

Central force orbit with  $a/b = 2$

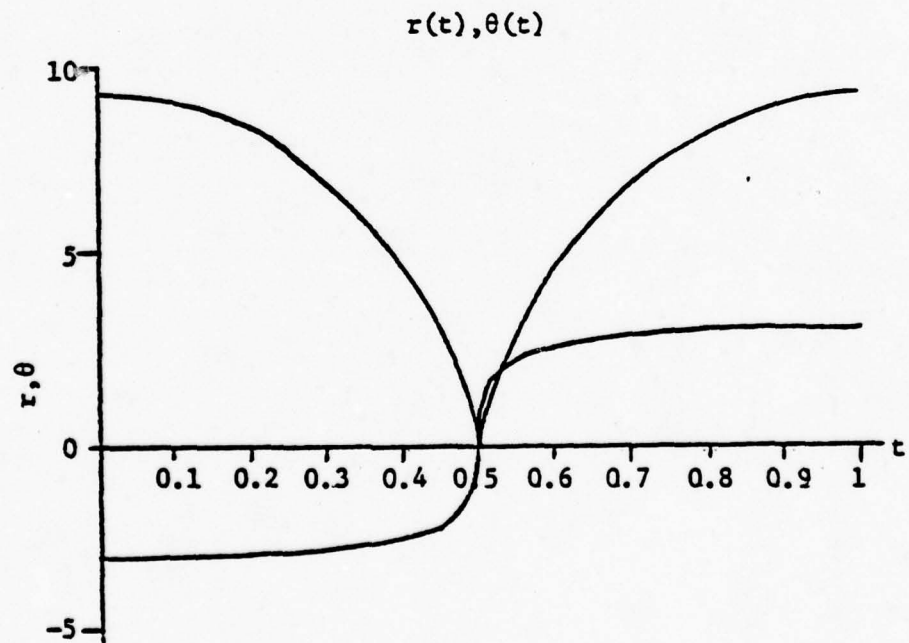
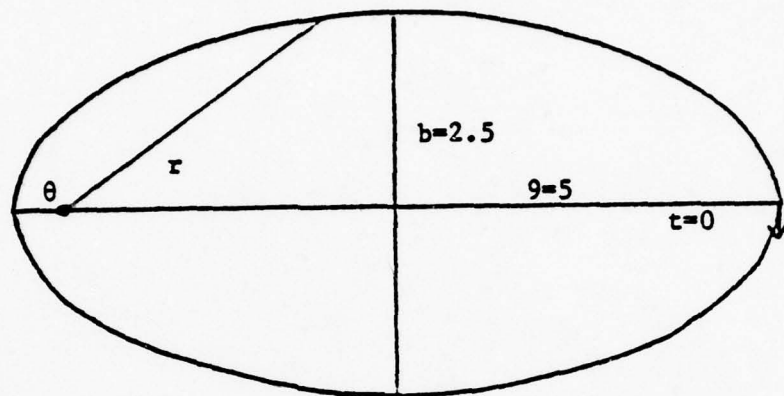


Figure 6. System 5 Exact Solution.

## V. TEST PROCEDURE

In all of the tests, the number of derivative evaluating subroutine calls (N), the CPU time of integration, and the maximum occurring error ( $\text{error}_{\max}$ ) were measured. (The solver DVOGER was used with both Adam's and Gear's methods and when it was used with Gear's method, the option was utilized in which the gradient of the derivative functions was evaluated numerically.)

All of the solvers, except RK45, require that an error tolerance (EPS) be given. For systems 1, 2, and 3, each integration was performed with  $\text{EPS} = 10^{-3}, 10^{-4}, 10^{-5}, 10^{-6}$ . For system 4, this was extended to  $10^{-12}$  and for system 5 to  $10^{-8}$ . RK45 was executed with a range of stepsizes which produced similar accuracy.

For the solvers which require a minimum stepsize,  $10^{-15}$  of the interval value was used. This corresponds to about 140 units of round-off.

All tests were executed in double precision.

## VI. RESULTS AND DISCUSSION

As mentioned previously, the primary interests are solver efficiency and accuracy. To discuss efficiency, it is desirable to consider the efficiency at a specified accuracy. Hence accuracy is discussed first.

The documentation of DRKGS and DHPCG state that the maximum global error,  $e_m$ , is usually of about the same magnitude as the specified error tolerance,  $\epsilon$ , but the documentations of the other solvers do not state that. To access the accuracy of the solvers  $e_m$  vs.  $\epsilon$  was plotted for several cases. Graphs 1 and 2 are typical of these results and deal with systems 1 and 5 respectively. Error estimation is clearly not exact and it is somewhat disappointing that  $e_m$  differed by a factor of 20 or 50 from  $\epsilon$  so frequently. From graph 1 alone, one might think that DHPCG is much superior to the other solvers in error estimation, but this is merely coincidence. There are other graphs where it appears to be poor and another appears to be good.

These graphs show only one value of stiffness and do not show if stiffness influences solver accuracy. Systems 1, 2 and 5 were specifically chosen because their stiffness could be varied in a desired manner. Graphs 3, 4 and 5 show explicitly how stiffness influences solver accuracy. These are graphs of  $(e_m/\epsilon)$  vs. stiffness. Graphs 3 and 4 deal with systems 1 and 2 respectively and hence Type 1 stiffness. Graph 5 deals with System 5 and Type 2 stiffness. In Graph 3, it appears that DREBS and DRKGS lose accuracy with increasing stiffness,



but that behavior is not confirmed by Graph 4. The other routines are not clearly affected by Type 1 stiffness and DVOGER appears to be the least influenced. However, a look at Graph 5 clearly shows that Type 2 stiffness is different. As the stiffness of the problem increases,  $e_m$  grows much larger than  $\epsilon$ .

Systems 3 and 4 contain Type 1 and Type 2 stiffness, respectively, and are even stiffer than the most stiff cases of systems 1, 2, and 5. Table 5 contains data pertinent to solver accuracy for systems 3 and 4. Note that  $e_m$  can be many orders of magnitude greater than  $\epsilon$ .

$(e_m/\epsilon)$ for very stiff systems		
	SYSTEM 3 (Type 1)	SYSTEM 4 (Type 2)
DRKGS	-	$1.2 \times 10^{12}$
DVOGER(GEAR)	4.6	$3.1 \times 10^{10}$
DVOGER(ADAMS)	-	$1.8 \times 10^{10}$
DREBS	-	$1.3 \times 10^8$
DHPCG	-	$2.3 \times 10^8$

Table 5. Error Ratio Data.

In every test integration, different solvers generated different accuracies, even when  $\epsilon$  was constant and hence, it is probably misleading to compare solver effort at equal  $\epsilon$ . Rather, it is probably more appropriate to compare solver effort at equal values of  $e_m$ . Graphs of  $N$  (the number of calls to the derivative evaluating subroutine) vs.  $e_m$  were prepared and estimates of  $N$  at a specific  $e_m$  were obtained. Usually these graphs were smooth and appeared to be hyperbolic (straight lines on log-log plots). Typical of these results is Graph 6 which pertains to System 5 and DRKGS. However, in some cases, these graphs were not smooth and Graph 7, concerning System 5 and DHPCG, shows such a result. In these cases, no attempt was made to estimate  $N$ .

In most of the tests, the solvers achieved  $10^{-5}$  accuracy and this value of  $e_m$  was chosen to compare solver efficiencies. Graphs 8, 9, and 10 pertain to Systems 1, 2, and 5, respectively. They show how stiffness influences integration effort. The effect is quite striking. The systems in Graphs 8 and 9 both contain Type 1 stiffness. Almost every routine requires more effort for the integration as stiffness increases. However, DVOGER (Gear) was specifically designed for systems with this type of stiffness and it is relatively unaffected by Type 1 stiffness. System 5 in Graph 10 contains Type 2 stiffness and it is clear that this stiffness increases integration effort. No routine was much more efficient than another in this problem. Rather, the true test was whether they could integrate all of the cases. Only DRKGS and DVOGER (Gear) achieved solutions accurate to  $10^{-5}$  for all stiffnesses.

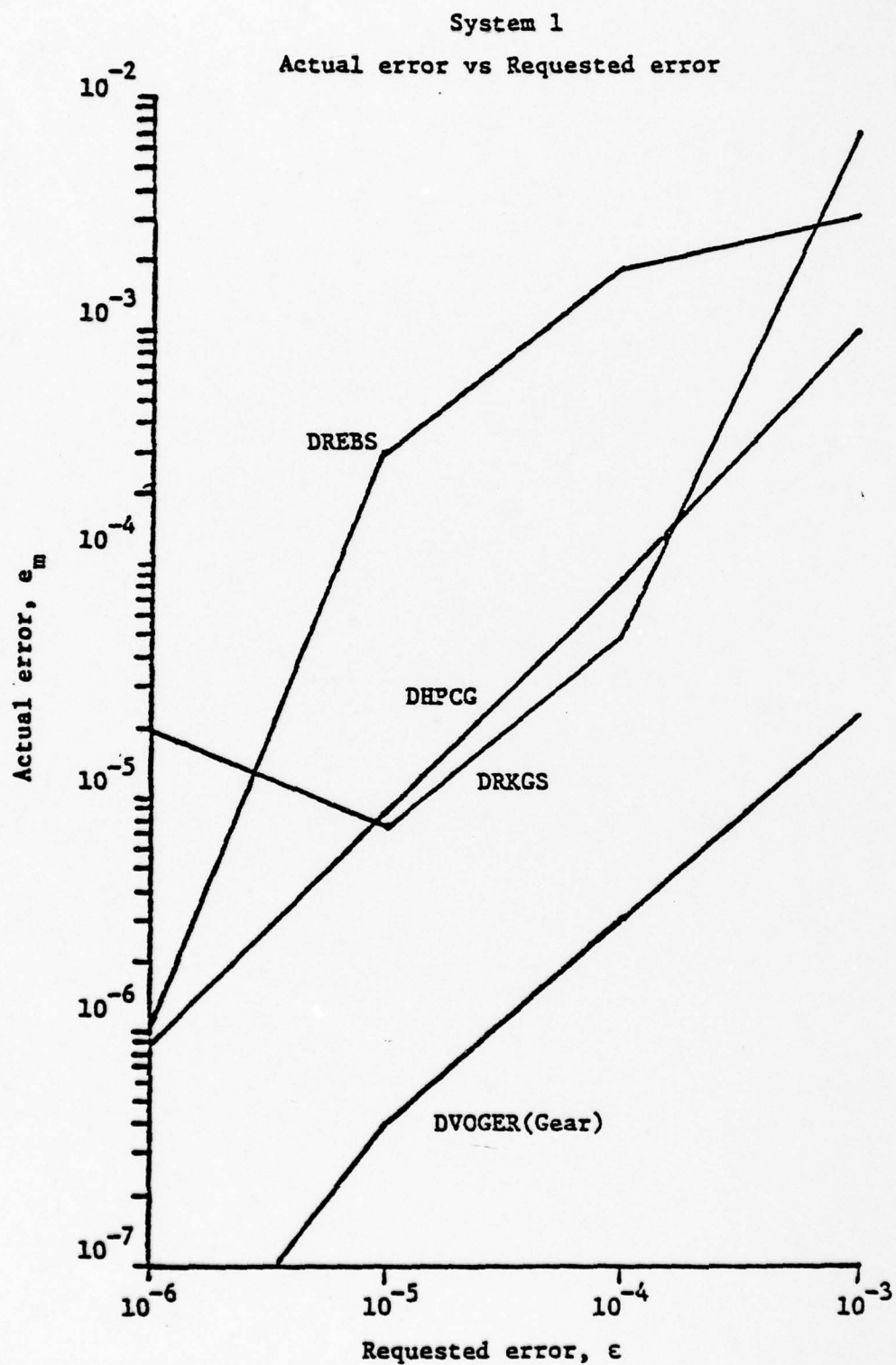
System 3, which had very much Type 1 stiffness could be solved to  $10^{-5}$  accuracy only by DVOGER (Gear). The other routines took so many

function evaluations that apparently roundoff error limited their accuracy. System 4, which had very much type 2 stiffness, was solved by DRKGS, DRK45, DREBS and DHPCG to  $10^{-3}$  relative error or better ( $10^{-2}$  was considered to be the minimum acceptable relative error). While DVOGER did not achieve this accuracy with absolute error control, it might perform better with relative error control. DHPCG achieved the best accuracy, about  $10^{-6}$ .

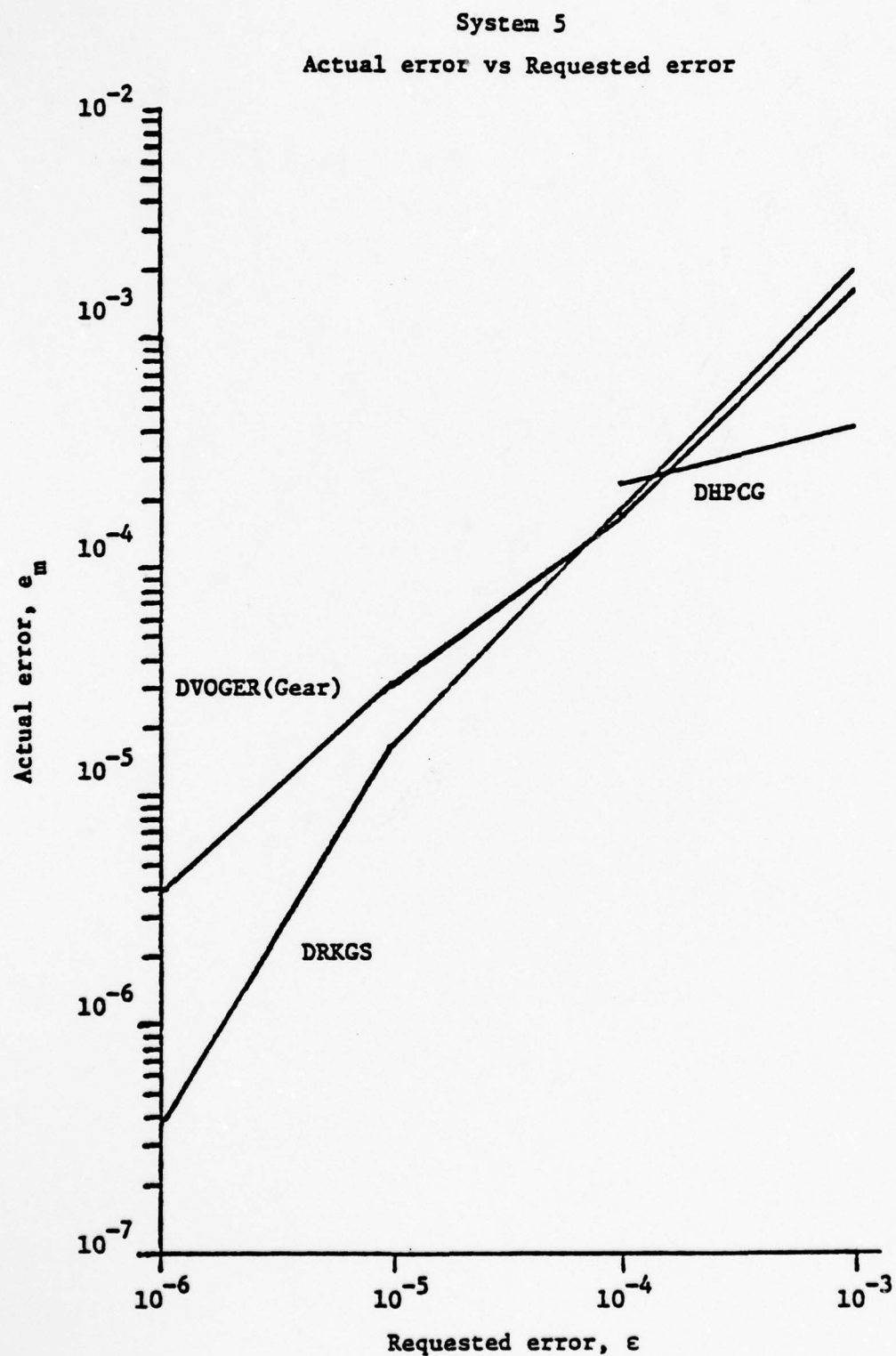
The CPU times of integration, T, were measured but they primarily represent overhead (time spent in the solver subroutine rather than the derivative evaluating subroutine). The overhead per derivative evaluation was computed and these values are shown in Table 6. For systems where the derivative evaluations are simple, these values of (T/N) may be used to convert results from N to T  
Graph 11 for the data from Graph 8 (System 1).

ROUTINE	CPU TIME PER DERIVATIVE SUBROUTINE CALL (μ-SEC)
DREBS	80
DRK45	103
DRKGS	106
DHPCG	220
DVOGER (ADAMS)	400
DVOGER (GEAR)	500

TABLE 6. CPU for Derivative Evaluation.

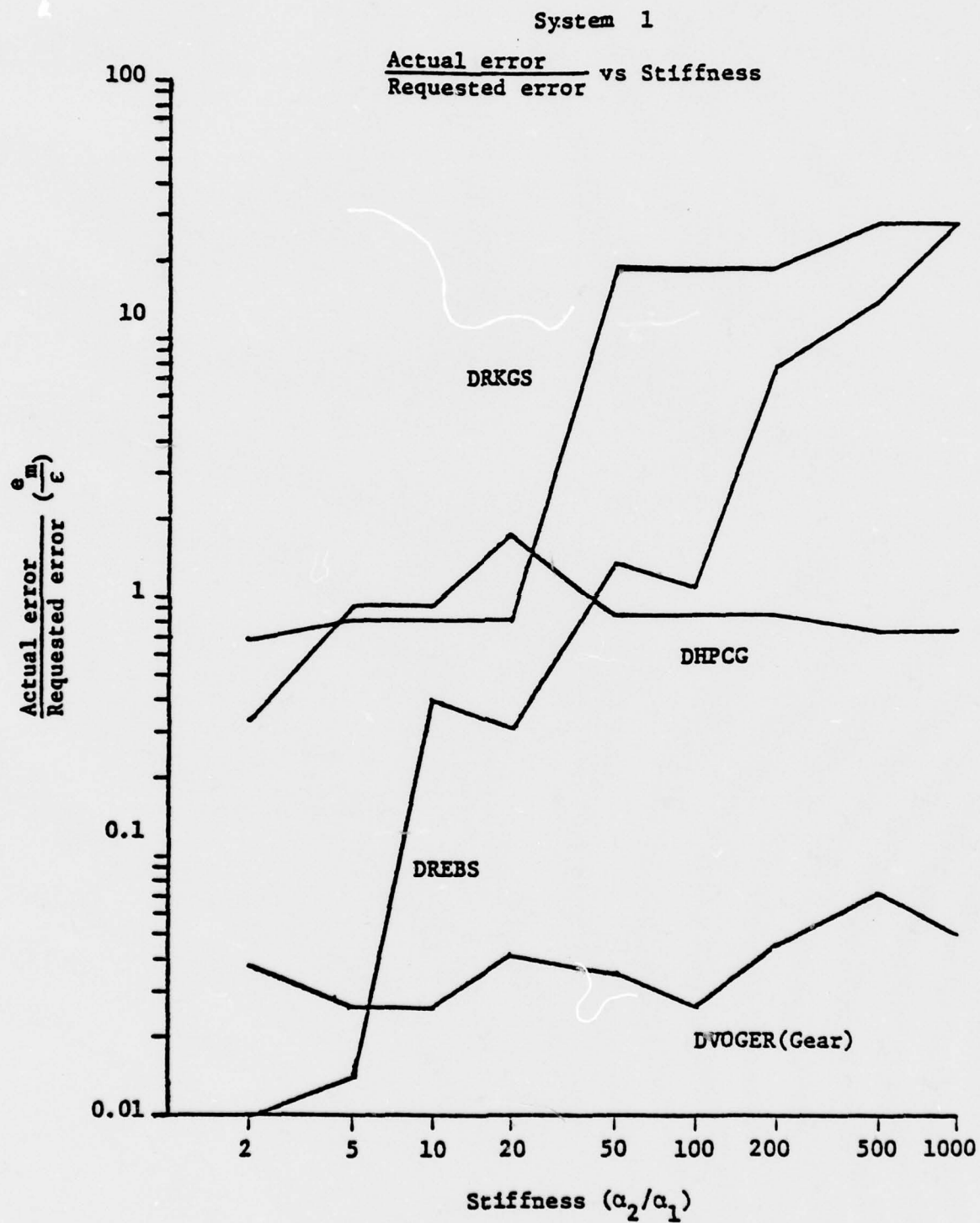


Graph 1. Actual Error vs. Requested Error - System 1.

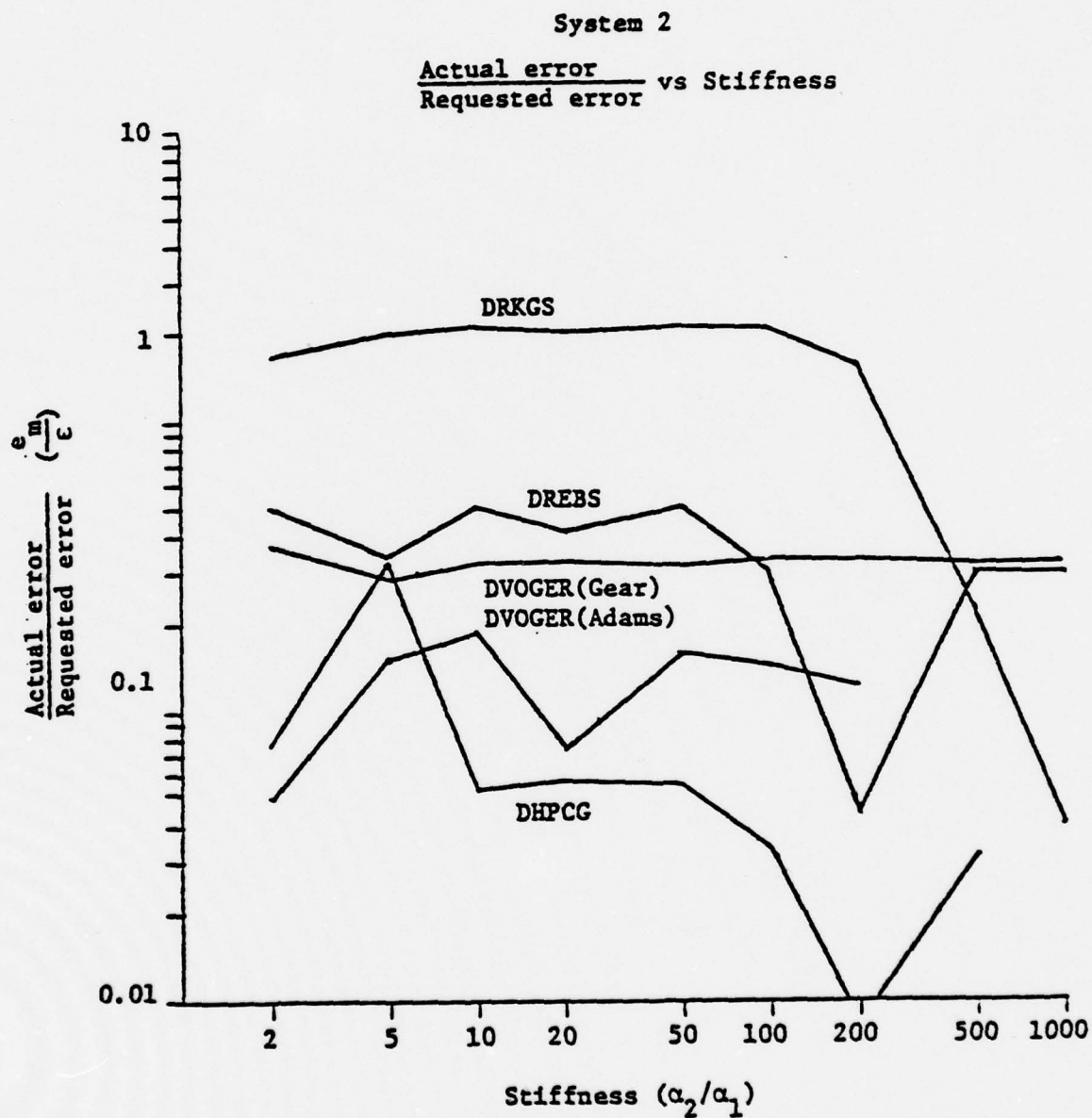


Graph 2. Actual Error vs. Requested Error - System 5.





Graph 3. Accuracy vs. Stiffness - System 1.



Graph 4. Accuracy vs. Stiffness - System 2.

## APPENDIX A

### EXACT SOLUTION TO THE DOUBLE-MASS-SPRING DASHPOT SYSTEM (SYSTEM 2)

The governing differential equations of motion for the system are:

$$m_1 \ddot{y}_1 + (c_1 + c_2) \dot{y}_1 - c_2 \dot{y}_2 + (k_1 + k_2) y_1 - k_2 y_2 = 0 \quad (A1)$$

and

$$m_2 \ddot{y}_2 - c_2 \dot{y}_1 + c_2 \dot{y}_2 - k_1 y_1 + k_2 y_2 = 0 \quad (A2)$$

Taking the Laplace transform of these equations and solving for  $y_1(s)$  and  $y_2(s)$  leads to:

$$y_1(s) = \frac{a_3 s^3 + a_2 s^2 + a_1 s + a_0}{d_4 (s^4 + d_3 s^3 + d_2 s^2 + d_1 s + d_0)} \quad (A3)$$

$$y_2(s) = \frac{b_3 s^3 + b_2 s^2 + b_1 s + b_0}{d_4 (s^4 + d_3 s^3 + d_2 s^2 + d_1 s + d_0)} \quad (A4)$$

where:

$$a_0 = c_1 k_2 y_1(0) + m_1 k_2 \dot{y}_1(0) + m_2 k_2 \dot{y}_2(0) \quad (A5)$$

$$a_1 = (m_1 k_2 + c_1 c_2) y_1(0) + m_2 k_2 y_2(0) + m_1 c_2 \dot{y}_1(0) + m_2 c_2 \dot{y}_2(0) \quad (A6)$$

$$a_2 = [m_1 c_2 + m_2 (c_1 + c_2)] y_1(0) + m_1 m_2 \dot{y}_1(0) \quad (A7)$$

$$a_3 = m_1 m_2 y_1(0) \quad (A8)$$

$$b_0 = (c_1 k_2 - c_2 k_1) y_1(0) + c_2 k_2 y_2(0) + m_1 k_2 \dot{y}_1(0) + m_2 (k_1 + k_2) \dot{y}_2(0) \quad (A9)$$

$$b_1 = m_1 k_2 y_1(0) + [m_2 (k_1 + k_2) + c_1 c_2] y_2(0) + m_1 c_2 \dot{y}_1(0) + m_2 (c_1 + c_2) \dot{y}_2(0) \quad (A10)$$

$$b_2 = -m_1 c_2 y_1(0) + [m_1 c_2 + m_2 (c_1 + c_2)] y_2(0) + m_1 m_2 \dot{y}_2(0) \quad (A11)$$

$$b_3 = m_1 m_2 y_2(0) \quad (A12)$$

$$d_0 = k_1 k_2 / d_4 \quad (A13)$$

$$d_1 = (c_1 k_2 + c_2 k_1) / d_4 \quad (A14)$$

$$d_2 = [m_1 k_2 + m_2 (k_1 + k_2) + c_1 c_2] / d_4 \quad (A15)$$

$$d_3 = [m_1 c_2 + m_2 (c_1 + c_2)] / d_4 \quad (A16)$$

$$d_4 = m_1 m_2 \quad (A17)$$

To "invert" the Laplace transform, it is convenient to break the expressions for  $y_1(s)$  and  $y_2(s)$  into partial fractions. If the mass-damper-spring system is underdamped, then solutions of the form  $e^{-\alpha t} \cos \omega t$  and  $e^{-\alpha t} \sin \omega t$  will exist. The inverse Laplace transforms of these functions are:

$$e^{-\alpha t} \cos \omega t \Leftrightarrow \frac{s + \alpha}{(s + \alpha)^2 + \omega^2} \quad (A18)$$

$$\frac{e^{-\alpha t} \sin \omega t}{\omega} \Leftrightarrow \frac{1}{(s + \alpha)^2 + \omega^2} \quad (A19)$$

Hence, it is necessary to factor the fourth order denominator into two quadratic terms. This was performed numerically with a computer routine for every case. Since all cases are underdamped the roots consist of two complex conjugate pairs:

$$- \alpha_1 \pm \omega_1 i \Leftrightarrow (s + \alpha_1 - \omega_1 i)(s + \alpha_1 + \omega_1 i) = (s + \alpha_1)^2 + \omega_1^2 \quad (A20)$$



and

$$-\alpha_2 \pm \omega_2 \Leftrightarrow (s + \alpha_2 - \omega_2)(s + \alpha_2 + \omega_2) = (s + \alpha_2)^2 + \omega_2^2 \quad (\text{A21})$$

Hence:

$$d_4 y_1(s) = \frac{e_1(st\alpha_1) + e_2}{(st\alpha_1)^2 + \omega_1^2} + \frac{e_3(st\alpha_2) + e_4}{(st\alpha_2)^2 + \omega_2^2} \quad (\text{A22})$$

$$d_4 y_2(s) = \frac{f_1(st\alpha_1) + f_2}{(st\alpha_1)^2 + \omega_1^2} + \frac{f_3(st\alpha_2) + f_4}{(st\alpha_2)^2 + \omega_2^2} \quad (\text{A23})$$

where  $e_1, e_2, e_3, e_4, f_1, f_2, f_3, f_4$  are determined by letting  $s$  approach  $-\alpha_1 \pm \omega_1 i$  and  $-\alpha_2 \pm \omega_2 i$ . This is equivalent to defining  $z_1, z_2, z_3$  and  $z_4$  as:

$$z_1 = \frac{a_3 s^3 + a_2 s^2 + a_1 s + a_0}{(st\alpha_2)^2 + \omega_2^2} \quad \text{with } s = -\alpha_1 + \omega_1 i \quad (\text{A24})$$

$$z_2 = \frac{a_3 s^3 + a_2 s^2 + a_1 s + a_0}{(st\alpha_1)^2 + \omega_1^2} \quad \text{with } s = \alpha_2 \pm \omega_2 i \quad (\text{A25})$$

$$z_3 = \frac{b_3 s^3 + b_2 s^2 + b_1 s + b_0}{(st\alpha_2)^2 + \omega_2^2} \quad \text{with } s = \alpha_1 \pm \omega_1 i \quad (\text{A26})$$

$$Z_4 = \frac{b_3 s^3 + b_2 s^2 + b_1 s + b_0}{(s + \alpha_1)^2 + \frac{\omega_1^2}{1}} \quad \text{with } s = \alpha_2 \pm \omega_s i \quad (\text{A27})$$

and then:

$$e_1 = \text{imag } Z_1 / \omega_1 \quad e_2 = \text{real } Z_1 \quad (\text{A28})$$

$$e_3 = \text{imag } Z_2 / \omega_2 \quad e_4 = \text{real } Z_2 \quad (\text{A29})$$

$$f_1 = \text{imag } Z_3 / \omega_1 \quad f_2 = \text{real } Z_3 \quad (\text{A30})$$

$$f_3 = \text{imag } Z_4 / \omega_2 \quad f_4 = \text{real } Z_4 \quad (\text{A31})$$

Finally,  $y_1(s)$  and  $y_2(s)$  can be "inverted", leading to the expressions:

$$\begin{aligned} y_1(t) = & e^{-\alpha_1 t} \left[ \frac{e_1}{d_4} \cos \omega_1 t + \frac{e_2}{d_4 \omega_1} \sin \omega_1 t \right] + \\ & + e^{-\alpha_2 t} \left[ \frac{e_3}{d_4} \cos \omega_2 t + \frac{e_4}{d_4 \omega_2} \sin \omega_2 t \right] \quad (\text{A32}) \end{aligned}$$

and

$$\begin{aligned}
 y_2(t) = & e^{-\alpha_1 t} \left[ \frac{f_1}{d_4} \cos \omega_1 t + \frac{f_2}{d_4 \omega_1} \sin \omega_1 t \right] \\
 & + e^{-\alpha_2 t} \left[ \frac{f_3}{d_4} \cos \omega_2 t + \frac{f_4}{d_4 \omega_2} \sin \omega_2 t \right]
 \end{aligned} \tag{A33}$$

These expressions can be written in the more convenient form:

$$y_1(t) = A_1 e^{-\alpha_1 t} \cos(\omega_1 t + \phi_1) + A_2 e^{-\alpha_2 t} \cos(\omega_2 t + \phi_2) \tag{A34}$$

$$y_2(t) = A_3 e^{-\alpha_1 t} \cos(\omega_1 t + \phi_3) + A_4 e^{-\alpha_2 t} \cos(\omega_2 t + \phi_4) \tag{A35}$$

where :

$$A_1 = [e_1^2 + (e_2/\omega_1)^2]^{1/2}/d_4 \tag{A36}$$

$$A_2 = [e_3^2 + (e_4/\omega_2)^2]^{1/2}/d_4 \tag{A37}$$

$$A_3 = [f_1^2 + (f_2/\omega_1)^2]^{1/2}/d_4 \tag{A38}$$

$$A_4 = [f_3^2 + (f_4/\omega_2)^2]^{1/2}/d_4 \tag{A39}$$

$$\phi_1 = -\tan^{-1} (e_2/e_1\omega_2) \quad (\text{A40})$$

$$\phi_2 = -\tan^{-1} (e_4/e_3\omega_2) \quad (\text{A41})$$

$$\phi_3 = -\tan^{-1} (f_2/f_1\omega_1) \quad (\text{A42})$$

$$\phi_4 = -\tan^{-1} (f_4/f_3\omega_2) \quad (\text{A43})$$

It is possible to choose  $m_1$ ,  $c_1$ ,  $k_1$ ,  $m_2$ ,  $c_2$  and  $k_2$  to obtain various desired values of  $\alpha_1$ ,  $\alpha_2$ ,  $\omega_1$  and  $\omega_2$ . The required relationships are simplified if the product  $m_1m_2$  is arbitrarily set to 1. Then the following four simultaneous nonlinear equations are obtained:

$$c_1 + 2c_2 = 2(\alpha_1 + \alpha_2) \quad (\text{A44})$$

$$k_1 + 2k_2 + c_1c_2 = \alpha_1^2 + \omega_1^2 + 4\alpha_1\alpha_2 + \alpha_2^2 + \omega_2^2 \quad (\text{A45})$$

$$c_1k_2 + c_2k_1 = 2[\alpha_1(\alpha_2^2 + \omega_2^2) + \alpha_2(\alpha_1^2 + \omega_1^2)] \quad (\text{A46})$$

$$k_1k_2 = (\alpha_1^2 + \omega_1^2)(\alpha_2^2 + \omega_2^2) \quad (\text{A47})$$

It is possible to solve these numerically for  $c_1$ ,  $c_2$ ,  $k_1$  and  $k_2$  (see Reference [19]). That is, let  $\underline{y}(\tau)$  be functions such that:

$$\underline{y}(\tau) = \begin{bmatrix} y_1(\tau) \\ y_2(\tau) \\ y_3(\tau) \\ y_4(\tau) \end{bmatrix} \quad (\text{A48})$$

and let

$$\underline{y}(0) = \begin{bmatrix} 2\alpha_1 \\ \alpha_1^2 + \omega_1^2 \\ 2\alpha_2 \\ \alpha_2^2 + \omega_2^2 \end{bmatrix} \quad (\text{A49})$$

Further, let

$$\underline{F}(\underline{y}) = \begin{bmatrix} y_1 + 2y_3 \\ y_2 + 2y_4 + y_1y_3 \\ y_1y_4 + y_3y_2 \\ y_2y_4 \end{bmatrix} - \begin{bmatrix} y_1(0) + y_3(0) \\ y_2(0) + y_1(0)y_3(0) + y_4(0) \\ y_1(0)y_4(0) + y_3(0)y_2(0) \\ y_2(0)y_4(0) \end{bmatrix} \quad (\text{A50})$$

Thus

$$\underline{F}(0) = \begin{bmatrix} y_3(0) \\ y_4(0) \\ 0 \\ 0 \end{bmatrix} \quad (\text{A51})$$



and

$$\underline{\nabla F} = \begin{bmatrix} 1 & 0 & 2 & 0 \\ y_3 & 1 & y_1 & 2 \\ y_4 & y_3 & y_2 & y_1 \\ 0 & y_4 & 0 & y_2 \end{bmatrix} \quad (\text{A52})$$

Finally, let

$$\underline{F}(\tau) = (1 - \tau)\underline{F}(0) \quad (\text{A53})$$

Then

$$\underline{F}(1) = 0 \quad (\text{A54})$$

and

$$\dot{\underline{F}}(\tau) = \underline{\nabla F} \dot{\underline{Y}} = -\underline{F}(0) \quad (\text{A55})$$

Hence,

$$\dot{\underline{Y}} = -[\underline{\nabla F}]^{-1}\underline{F}(0) \quad (\text{A56})$$

Equations (A56) form a system of four first order differential equations whose solution  $y(\tau)$  evaluated at  $\tau = 1$ , provide the desired values of  $c_1$ ,  $k_1$ ,  $c_2$ , and  $k_2$ .

APPENDIX B

Solver Subroutine Listings

```

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45
***
SUBROUTINE DRK45(X,XDOT,I,H,M)
  IMPLICIT REAL*8 (A-H,O-Z)
  RUNGE-KUTTA OPTIMAL COEFFS ROUTINE.  TRUNCATION ERROR = H**6.
  H = STEP SIZE
  M = NUMBER OF FIRST ORDER DIFFERENTIAL EQUATIONS
  I = INDEPENDENT VARIABLE
  X IS THE STATE VECTOR
  XDOT IS THE DERIVATIVE OF THE STATE VECTOR X
  THE VECTORS X(I+H) AND XDOT(I+H) ARE RETURNED
  RK45 CALLS XDOTEQ(X,XDOT,I) WHICH IS THE SUBROUTINE IN
  WHICH THE M FIRST ORDER EQUATIONS ARE INPUT..
  XDOTEQ INPUT IS AS FOLLOWS
    XDOT(1) = F(X,I)
    XDOT(2) = G(X,I)
    ETC.

  DIMENSION X(M),XDOT(M),XNEW(20),A(6),F(6,20),SAVE(20),B(6,5)
  DATA KJNT/0/
  IF(KJNT.GT.0) GO TO 5
  KJNT=1
  A(1)=0.0D0
  A(2)=.3D0
  A(3)=.3D0
  A(4)=.6D0
  A(5)=1.0D0
  A(6)=1.0D0/12.0D0
  C1=59.50D0/594.0D0
  C4=27.50D0/693.0D0
  C5=12.50D0/513.0D0
  C6=-1.62D0/773.0D0
  H(2,1)=3.2D0
  H(3,1)=3.0D0/40.0D0
  H(5,2)=9.0D0/40.0D0
  B(4,1)=.3D0
  B(4,2)=1.2D0
  B(4,3)=1.0D0/54.0D0
  B(5,1)=2.5D0
  B(5,2)=7.0D0/27.0D0
  B(5,3)=35.0D0/27.0D0
  B(6,1)=-473.0D0/10368.0D0
  B(6,2)=1595.0D0/1728.0D0
  B(6,3)=-34595.0D0/54432.0D0
  30.
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46 B(6,4)=38665,D0/62208,D0
47 H(6,5)=7733,D0/145152,D0
48 DO 4 J=1,M
49 XSAVE(J)=0,000
50 XSAVE(J)=X(J)
51 DO 10 K=1,6
52 IF(K, EQ, 1) GO TO 30
53 NEK=J
54 DO 20 J=1,M
55 XSAVE(J)=0,000
56 DO 40 LAM=1,2,N
57 XSAVE(J)=SAVE(J)+B(K,LAM)*F(LAM,J)
58 DO 30 J=1,M
59 XNEW(N)=XSAVE(N)+SAVE(N)
60 INEW=T+A(K)*H
61 CALL XDOTEQ(XNEW,XDOT,INEW)
62 DO 60 J=1,M
63 F(K,J)=XDOT(J)
64 CONF=VUE
65 DO 70 J=1,M
66 X(J)=XSAVE(J)+H*(C1*F(1,J)+C3*F(3,J)+C4*F(4,J)+C5*F(5,J)+
67 C6*F(6,J))
68 I=I+H
69 RETURN
70 END
71

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SUBROUTINE DRKGS(PRMT,Y,DERY,NDIM,IHLF,FCT,OUTP,AUX)

PURPOSE  
TO SOLVE A SYSTEM OF FIRST ORDER ORDINARY DIFFERENTIAL  
EQUATIONS WITH GIVEN INITIAL VALUES.

USAGE  
CALL DRKGS (PRMT,Y,DERY,NDIM,IHLF,FCT,OUTP,AUX)  
PARAMETERS FCT AND OUTP REQUIRE AN EXTERNAL STATEMENT.

DESCRIPTION OF PARAMETERS  
PRMT -  
DOUBLE PRECISION INPUT AND OUTPUT VECTOR WITH  
DIMENSION GREATER THAN OR EQUAL TO 5, WHICH  
SPECIFIES THE PARAMETERS OF THE INTERVAL AND OF  
ACCURACY AND WHICH SERVES FOR COMMUNICATION BETWEEN  
OUTPUT SUBROUTINE (FURNISHED BY THE USER) AND  
SUBROUTINE DRKGS. EXCEPT PRMT(5) THE COMPONENTS  
ARE NOT DESTROYED BY SUBROUTINE DRKGS AND THEY ARE  
PRMT(1) - LOWER BOUND OF THE INTERVAL (INPUT),  
PRMT(2) - UPPER BOUND OF THE INTERVAL (INPUT),  
PRMT(3) - INITIAL INCREMENT OF THE INDEPENDENT VARIABLE  
(INPUT),  
PRMT(4) - UPPER ERROR BOUND (INPUT), IF ABSOLUTE ERROR IS  
GREATER THAN PRMT(4), INCREMENT GETS HALVED.  
IF INCREMENT IS LESS THAN PRMT(3) AND ABSOLUTE  
ERROR LESS THAN PRMT(4)/50 INCREMENT GETS DOUBLED.  
THE USER MAY CHANGE PRMT(4) BY MEANS OF HIS  
OUTPUT SUBROUTINE.  
PRMT(5) - NO INPUT PARAMETER. SUBROUTINE DRKGS INITIALIZES  
PRMT(5)=0. IF THE USER WANTS TO TERMINATE  
SUBROUTINE DRKGS AT ANY OUTPUT POINT, HE HAS TO  
CHANGE PRMT(5) TO NON-ZERO BY MEANS OF SUBROUTINE  
OUTPUT. FURTHER COMPONENTS OF VECTOR PRMT ARE  
FEASIBLE IF ITS DIMENSION IS DEFINED GREATER  
THAN 5. HOWEVER SUBROUTINE DRKGS DOES NOT REQUIRE  
AND CHANGING THEM. NEVERTHELESS THEY MAY BE USEFUL  
FOR HANDLING RESULTS WHICH ARE OBTAINED BY PROGRAM  
(CALLING DRKGS) WHICH ARE OBTAINED BY SPECIAL  
MANIPULATIONS WITH OUTPUT DATA IN SUBROUTINE QUIP.  
DOUBLE PRECISION WITH INPUT VECTOR OF INITIAL VALUES  
(DESTROYED). LATERON Y IS THE RESULTING VECTOR OF  
DEPENDENT VARIABLES COMPILED AT INTERMEDIATE  
POINTS X.  
DERY - DOUBLE PRECISION INPUT VECTOR OF ERROR WEIGHTS  
(DESTROYED). THE SUM OF ITS COMPONENTS MUST BE



490 DRKG  
500 DRKG  
510 DRKG  
520 DRKG  
530 DRKG  
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770 DRKG  
780 DRKG  
790 DRKG  
800 DRKG  
810 DRKG  
820 DRKG  
830 DRKG  
840 DRKG  
850 DRKG  
860 DRKG  
870 DRKG  
880 DRKG  
890 DRKG  
900 DRKG  
910 DRKG  
920 DRKG  
930 DRKG

EQUAL TO 1, LATERON DERY IS THE VECTOR OF  
DERIVATIVES, WHICH BELONG TO FUNCTION VALUES Y AT  
INTERMEDIATE POINTS X. SPECIFIES THE NUMBER OF  
AN INPUT VALUE, WHICH SPECIFIES THE NUMBER OF  
EQUATIONS IN THE SYSTEM, SPECIFIES THE NUMBER OF  
BISECTIONS OF THE INITIAL INCREMENT, IF IHLF GETS  
GREATER THAN 10, SUBROUTINE DRKGS RETURNS WITH  
ERROR MESSAGE IHLF=11 INTO MAIN PROGRAM, ERROR  
MESSAGE IHLF=12 OR IHLF=13 APPEARS IN CASE  
PRMT(3)=0 OR IN CASEY.  
PRMT(3)=0 OR IN CASEY.  
PRMT(1) RESPECTIVELY.  
THE NAME OF AN EXTENSIONAL SUBROUTINE USED. THIS  
SUBROUTINE COMPUTES THE RIGHT HAND SIDES DERY OF  
THE SYSTEM TO GIVEN VALUES X AND Y, ITS PARAMETER  
LIST MUST BE X,Y,DERY. SUBROUTINE FCI SHOULD  
NOT DESTROY X AND Y.  
THE NAME OF AN EXTENSIONAL SUBROUTINE USED.  
ITS PARAMETER LIST MUST BE X,Y,DERY, IHLF,NDIM,PRMT.  
MOVE OF THESE PARAMETERS (EXCEPT, IF NECESSARY,  
PRMT(4), PRMT(5)). IF PRMT(5) IS CHANGED TO NON-ZERO,  
SUBROUTINE DUTP IS TERMINATED.  
SUBROUTINE DRKGS IS TERMINATED.  
DOUBLE PRECISION AUXILIARY STORAGE ARRAY WITH 8  
RUNS AND NDIM COLUMNS.

NDIM  
IHLF  
FCI  
DUTP  
AUX

REMARKS  
THE PROCEDURE TERMINATES AND RETURNS TO CALLING PROGRAM, IF  
(1) MORE THAN 10 BISECTIONS OF THE INITIAL INCREMENT ARE  
NECESSARY TO GET SATISFACTORY ACCURACY (ERROR MESSAGE  
IHLF=11), INCREMENT IS EQUAL TO 0 OR HAS WRONG SIGN  
(2) INITIAL MESSAGE IHLF=12 OR IHLF=13,  
(3) THE WHOLE INTEGRATION INTERVAL IS WORKED THROUGH,  
(4) SUBROUTINE DUTP HAS CHANGED PRMT(5) TO NON-ZERO.  
SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED  
THE EXTERNAL SUBROUTINES FC(X,Y,DERY) AND  
DUTP(X,Y,DERY,IHLF,NDIM,PRMT) MUST BE FURNISHED BY THE USER.  
METHOD  
EVALUATION IS DONE BY MEANS OF FOURTH ORDER RUNGE-KUTTA  
FORMULAE IN THE MODIFICATION DUE TO GILL. ACCURACY IS  
TESTED COMPARING THE RESULTS OF THE PROCEDURE WITH SINGLE  
AND DOUBLE INCREMENT.

46 C  
47 C  
48 C  
49 C  
50 C  
51 C  
52 C  
53 C  
54 C  
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57 C  
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86 C  
87 C  
88 C  
89 C  
90 C

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91 CCCCCCCCCCCCCCCCCC
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SUBROUTINE DRKGS AUTOMATICALLY ADJUSTS THE INCREMENT DURING
THE WHOLE COMPUTATION BY HALVING OR DOUBLING. IF MORE THAN
10 BISECTIONS OF THE INCREMENT ARE NECESSARY TO GET
SATISFACTORY ACCURACY, THE SUBROUTINE RETURNS WITH
ERROR MESSAGE IHLF=11 INTO MAIN PROGRAM.
TO GET FULL FLEXIBILITY IN OUTPUT, AN OUTPUT SUBROUTINE
MUST BE FURNISHED BY THE USER.
FOR REFERENCE, SEE
HALSTON/WILF, MATHEMATICAL METHODS FOR DIGITAL COMPUTERS,
WILEY, NEW YORK/LONDON, 1960, PP.110-120.
.....
DIMENSION Y(NDIM), DERY(NDIM), AUX(8,NDIM), A(4), B(4), C(4), PRMT(5),
DOUBLE PRECISION PRMT, Y, DERY, AUX, A, B, C, X, XEND, H, AJ, BJ, CJ, RI, K2,
IDELT, DABS
DO I=1,NDIM
1 AUX(8,I)=.06666666666666667 D0*DERY(I)
X=PRMT(1)
XEND=PRMT(2)
H=PRMT(3)
PRMT(5)=0.D0
CALL FCT(X,Y,DERY)
ERROR TEST
IF(H*(XEND-X))38,37,2
PREPARATIONS FOR RUNGE-KUTTA METHOD
A(1)=.500
A(2)=.2928932188134525 D0
A(3)=1.707106781186548 D0
A(4)=1.6666666666666667 D0
B(1)=2.D0
B(2)=1.D0
B(3)=1.D0
B(4)=2.D0
C(1)=.500
C(2)=.2928932188134525 D0
C(3)=1.707106781186548 D0
C(4)=.500
PREPARATIONS OF FIRST RUNGE-KUTTA STEP
DO 3 I=1,NDIM

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136      C C C
137      C C
138      C C
139      C C
140      C C
141      C C
142      C C
143      C C
144      C C
145      C C
146      C C
147      C C
148      C C
149      C C
150      C C
151      C C
152      C C
153      C C
154      C C
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170      C C
171      C C
172      C C
173      C C
174      C C
175      C C
176      C C
177      C C
178      C C
179      C C
180      C C

      AUX(1,1)=Y(I)
      AUX(2,1)=DERY(I)
      AUX(3,1)=0.00
      3  AUX(6,1)=0.00
      H=H+H
      IHLE=-1
      ISTEP=0
      IEND=0

      START OF A RUNGE-KUTTA STEP
      4  IF((X+H-XEND)*H)7,6,5
      5  H=XEND-X
      6  IEND=1

      RECORDING OF INITIAL VALUES OF THIS STEP
      7  CALL CJTP(X,Y,DERY,IREC,NDIM,PRMT)
      8  IF(PRMT(5))40,8,40
      9  ITEST=0
      9  ISTEP=ISTEP+1

      START OF INNERMOST RUNGE-KUTTA LOOP
      10 J=1
      10 AJ=A(J)
      10 BJ=B(J)
      10 CJ=C(J)
      10 DO 11 I=1,NDIM
      10 R1=H*DERY(I)
      10 R2=AJ*(R1-HJ*AUX(6,I))
      10 Y(I)=Y(I)+R2
      10 R2=R2+R2+R2
      11 AUX(6,I)=AUX(6,I)+R2-CJ*R1
      11 IF(J-4)12,15,15
      12 J=J+1
      12 IF(J-3)13,14,13
      13 X=X+H*SD0*H
      14 CALL FCI(X,Y,DERY)
      14 GOTO 10
      15 END OF INNERMOST RUNGE-KUTTA LOOP

      TEST OF ACCURACY
      15 IF(ITEST)16,16,20

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181 C
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IN CASE ITEST=0 THERE IS NO POSSIBILITY FOR TESTING OF ACCURACY
16 DO 17 I=1,NDIM
17 AUX(4,I)=Y(I)
18 ITEST=1
18 ISTEP=ISTEP+ISTEP-2
18 IHLF=IHLF+1
18 X=X-H
18 H=.5D0*H
18 DO 19 I=1,NDIM
18 Y(I)=AJX(I,1)
18 DERY(I)=AUX(2,I)
18 AUX(6,I)=AUX(3,I)
18 GO TO 9

IN CASE ITEST=1 TESTING OF ACCURACY IS POSSIBLE
20 IMOD=ISTEP/2
20 IF(ISTEP-IMOD-IMOD)21,23,21
21 CALL FCT(X,Y,DERY)
21 DO 22 I=1,NDIM
21 AUX(5,I)=Y(I)
21 AUX(7,I)=DERY(I)
21 GO TO 9

COMPUTATION OF TEST VALUE DELT
23 DELT=0.00
23 DO 24 I=1,NDIM
23 DELT=DELT+AUX(8,I)*DABS(AUX(4,I)-Y(I))
24 IF(DELT-PRMT(4))28,28,25

ERROR IS TOO GREAT
25 IF(IHLF-30)26,56,56
26 DO 27 I=1,NDIM
27 AUX(4,I)=AUX(5,I)
27 ISTEP=ISTEP+ISTEP-4
27 X=X-H
27 IEND=0
27 GO TO 18

RESULT VALUES ARE GOOD
28 CALL FCT(X,Y,DERY)
28 DO 29 I=1,NDIM
28 AUX(1,I)=Y(I)
28 AUX(2,I)=DERY(I)
28 AUX(3,I)=AUX(6,I)

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DRKG1850
DRKG1860
DRKG1870
DRKG1880
DRKG1890
DRKG1900
DRKG1910
DRKG1920
DRKG1930
DRKG1940
DRKG1950
DRKG1960
DRKG1970
DRKG1980
DRKG1990
DRKG2000
DRKG2010
DRKG2020
DRKG2030
DRKG2040
DRKG2050
DRKG2060
DRKG2070
DRKG2080
DRKG2090
DRKG2100
DRKG2110
DRKG2120
DRKG2130
DRKG2140
DRKG2150
DRKG2160
DRKG2170
DRKG2180
DRKG2190
DRKG2200
DRKG2210
DRKG2220
DRKG2230
DRKG2240
DRKG2250
DRKG2260
DRKG2270
DRKG2280
DRKG2290

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DRKG2300  
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 DRKG2470  
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 DRKG2490  
 DRKG2500  
 DRKG2510  
 DRKG2520  
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29  Y(I)=AUX(5,I)
    DERY(I)=AUX(7,I)
    CALL JUIP(X,H,Y,DERY,IHLF,NDIM,PRMT)
30  IF (PRMT(5)) 40,30,40
    DO 31 I=1,NDIM
31  Y(I)=AUX(1,I)
    DERY(I)=AUX(2,I)
    IREC=IHLF
    IF (IEVD) 32,32,39
32  INCREMENT GETS DOUBLED
    IHLF=IHLF-1
    ISTEP=ISTEP/2
    H=H+H
    IF (IHLF) 4,33,33
33  IMOD=ISTEP/2
    IF (IMOD-IMOD) 4,34,4
34  IF (DELT-0.0200*PRMT(4)) 35,35,4
35  IHLF=IHLF-1
    ISTEP=ISTEP/2
    H=H+H
    GO TO 4

    RETURNS TO CALLING PROGRAM
36  IHLF=31
    CALL FCT(X,Y,DERY)
37  GO TO 39
    IHLF=32
38  GO TO 39
    IHLF=33
39  CALL JUIP(X,Y,DERY,IHLF,NDIM,PRMT)
40  RETURN
    END
  
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1  SUBROUTINE DHPG(PRMT,Y,DERY,NDIM,IHLF,FCI,UUIP,AUX)
2
3  PURPOSE
4  TO SOLVE A SYSTEM OF FIRST ORDER ORDINARY GENERAL
5  DIFFERENTIAL EQUATIONS WITH GIVEN INITIAL VALUES.
6
7  USAGE
8  CALL DHPG (PRMT,Y,DERY,NDIM,IHLF,FCI,OUTP,AUX)
9  PARAMETERS FCI AND OUTP REQUIRE AN EXTERNAL STATEMENT.
10
11  DESCRIPTION OF PARAMETERS
12  PRMT - DOUBLE PRECISION INPUT AND OUTPUT VECTOR WITH
13         DIMENSION GREATER THAN OR EQUAL TO 5, WHICH
14         SPECIFIES THE PARAMETERS OF THE INTERVAL AND OF
15         ACCURACY AND WHICH SERVES FOR COMMUNICATION BETWEEN
16         OUTPUT SUBROUTINE (FURNISHED BY THE USER) AND
17         SUBROUTINE DHPG, EXCEPT PRMT(5) THE COMPONENTS
18         ARE NOT DESTROYED BY SUBROUTINE DHPG AND THEY ARE
19         LOWER BOUND OF THE INTERVAL (INPUT),
20         UPPER BOUND OF THE INTERVAL (INPUT),
21         INITIAL INCREMENT OF THE INDEPENDENT VARIABLE
22         (INPUT),
23         UPPER ERROR BOUND (INPUT). IF ABSOLUTE ERROR IS
24         GREATER THAN PRMT(4), INCREMENT GETS HALVED.
25         IF INCREMENT IS LESS THAN PRMT(3) AND ABSOLUTE
26         ERROR LESS THAN PRMT(4)/50, INCREMENT GETS DOUBLED.
27         THE USER MAY CHANGE PRMT(4) BY MEANS OF HIS
28         OUTPUT SUBROUTINE.
29         NO INPUT PARAMETER. SUBROUTINE DHPG INITIALIZES
30         PRMT(5)=0. IF THE USER WANTS TO TERMINATE
31         SUBROUTINE DHPG AT ANY OUTPUT POINT, HE HAS TO
32         CHANGE PRMT(5) TO NON-ZERO BY MEANS OF SUBROUTINE
33         OUTPUT. FURTHER COMPONENTS OF VECTOR PRMT ARE
34         FEASIBLE IF ITS DIMENSION IS DEFINED GREATER
35         THAN 5. HOWEVER SUBROUTINE DHPG DOES NOT REQUIRE
36         AND CHANGE THEM. NEVERTHELESS THEY MAY BE USEFUL
37         FOR HANDLING RESULT VALUES TO THE MAIN PROGRAM
38         (CALLING DHPG) WHICH ARE OBTAINED BY SPECIAL
39         MANIPULATIONS WITH OUTPUT DATA IN SUBROUTINE DHPG.
40         DOUBLE PRECISION INPUT VECTOR OF INITIAL VALUES
41         (DESTROYED). LATERON Y IS THE RESULTING VECTOR OF
42         DEPENDENT VARIABLES COMPUTED AT IMMEDIATE
43         POINTS X
44         DOUBLE PRECISION INPUT VECTOR OF ERROR WEIGHTS
45         (DESTROYED). THE SUM OF ITS COMPONENTS MUST BE

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FOURTH ORDER RUNGE-KUITA METHOD SUGGESTED BY KALSTON IS
USED FOR ADJUSTMENT OF THE INITIAL INCREMENT AND FOR
COMPUTATION OF STARTING VALUES.
SUBROUTINE DHPCC AUTOMATICALLY ADJUSTS THE INCREMENT DUKING
THE WHOLE COMPUTATION BY HALVING OR DOUBLING.
TO GET FULL FLEXIBILITY IN OUTPUT, AN OUTPUT SUBROUTINE
MUST BE CODED BY THE USER.
FOR REFERENCE, SEE MATHEMATICAL METHODS FOR DIGITAL
(1) RALSTON/WILF, WILEY, NEW YORK/LONDON, 1960, PP.95-109.
(2) KALSTON, RUNGE-KUITA METHODS WITH MINIMUM ERROR BOUNDS,
MIAC, VOL.16, ISS.80 (1962), PP.431-437.
.....
DIMENSION PRMT(5),Y(NDIM),DERY(NDIM),AUX(16,NDIM)
DOUBLE PRECISION Y,DERY,AUX,PRMT,X,H,Z,DEL,DABS
N=1
IHLF=0
X=PRMT(1)
H=PRMT(3)
PRMT(5)=0.D0
DO 1 I=1,NDIM
AUX(16,I)=0.D0
AUX(15,I)=DERY(I)
AUX(14,I)=Y(I)
1 AUX(1,I)=Y(I)
IF(CH*(PRMT(2)-X))3,2,4
ERROR RETURNS
2 IHLF=22
GOTO 4
3 IHLF=23
COMPUTATION OF DERY FOR STARTING VALUES
4 CALL FCI(X,Y,DERY)
RECORDING OF STARTING VALUES
CALL UJIP(X,Y,DERY,IHLF,NDIM,PRMT)
IF(PRMT(5))6,5,6
5 IF(IHLF)7,7,6
6 REIKV
7 DO 8 I=1,NDIM
8 AUX(8,I)=DERY(I)
DHC6 940
DHC6 950
DHC6 960
DHC6 970
DHC6 980
DHC6 990
DHC6 1000
DHC6 1010
DHC6 1020
DHC6 1030
DHC6 1040
DHC6 1050
DHC6 1060
DHC6 1070
DHC6 1080
DHC6 1090
DHC6 1100
DHC6 1110
DHC6 1140
DHC6 1150
DHC6 1160
DHC6 1170
DHC6 1180
DHC6 1190
DHC6 1200
DHC6 1210
DHC6 1220
DHC6 1230
DHC6 1240
DHC6 1250
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DHC6 1270
DHC6 1280
DHC6 1290
DHC6 1300
DHC6 1310
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DHC6 1330
DHC6 1340
DHC6 1350
DHC6 1360
DHC6 1370
DHC6 1380
DHC6 1390

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DHCG1400  
DHCG1410  
DHCG1420  
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DHCG1500  
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DHCG1590  
DHCG1600  
DHCG1610  
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DHCG1660  
DHCG1670  
DHCG1680  
DHCG1690  
DHCG1700  
DHCG1710  
DHCG1720  
DHCG1730  
DHCG1740  
DHCG1750  
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DHCG1770  
DHCG1780  
DHCG1790  
DHCG1800  
DHCG1810  
DHCG1820  
DHCG1830  
DHCG1840

```

136 C      COMPUTATION OF AUX(2,1)
137 C      ISW=1
138 C      GUID 100
139 C
140 C
141 C      9 X=X+H
142 C      DO 10 I=1,NDIM
143 C      10 AUX(2,I)=Y(I)
144 C
145 C      INCREMENT H IS TESTED BY MEANS OF BISECTION
146 C      11 IHLF=IHLF+1
147 C      X=X-H
148 C      DO 12 I=1,NDIM
149 C      12 AUX(4,I)=AUX(2,I)
150 C      H=.500*H
151 C      N=1
152 C      ISW=2
153 C      GUID 100
154 C
155 C      13 X=X+H
156 C      CALL FCI(X,Y,DERY)
157 C      N=2
158 C      DO 14 I=1,NDIM
159 C      14 AUX(2,I)=Y(I)
160 C      AUX(9,I)=DERY(I)
161 C      ISW=3
162 C      GUID 100
163 C
164 C      COMPUTATION OF TEST VALUE DELT
165 C      DELT=0,DO
166 C      DO 16 I=1,NDIM
167 C      16 DELT=DELT+AUX(15,I)*DABS(Y(I)-AUX(4,I))
168 C      DELT=.066666666666666667/DO*DELT
169 C      IF(DELT-PRMT(4))19,19,17
170 C      17 IF(IHLF-20)11,16,18
171 C
172 C      NO SATISFACTORY ACCURACY AFTER 10 BISECTIONS. ERROR MESSAGE.
173 C      18 IHLF=21
174 C      X=X+H
175 C      GUID 4
176 C
177 C      THERE IS SATISFACTORY ACCURACY AFTER LESS THAN 11 BISECTIONS.
178 C      19 X=X+H
179 C      CALL FCI(X,Y,DERY)
180 C      DO 20 I=1,NDIM

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DHCG1850  
DHCG1860  
DHCG1870  
DHCG1880  
DHCG1890  
DHCG1900  
DHCG1910  
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DHCG1950  
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DHCG2120  
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DHCG2190  
DHCG2200  
DHCG2210  
DHCG2220  
DHCG2230  
DHCG2240  
DHCG2250  
DHCG2260  
DHCG2270  
DHCG2280  
DHCG2290

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181      AUX(3,I)=Y(I)
182      AUX(10,I)=DERY(I)
183      N=3
184      ISW=4
185      GUID 100
186
187      C
188
189      21  N=1
190      X=X+H
191      CALL FC1(X,Y,DERY)
192      X=PRMT(1)
193      DO 22 I=1,NDIM
194      AUX(1,I)=DERY(I)
195      220 Y(1)=AUX(1,I)+H*(.375D0*AUX(8,I)+.7916666666666667D0*AUX(9,I)
196      1-.20H3333333333333333D0*AUX(10,I)+.041666666666666667D0*DERY(I))
197      23  X=X+H
198      W=N+1
199      CALL FC1(X,Y,DERY)
200      CALL QJIP(X,Y,DERY,IHLF,NDIM,PRMT)
201      IF(PRMT(5))6,24,6
202      IF(N-4)25,200,200
203      DO 26 I=1,NDIM
204      AUX(N,I)=Y(I)
205      AUX(N+1,I)=DERY(I)
206      IF(N-3)27,29,200
207
208      27  DO 28 I=1,NDIM
209      DELT=AUX(9,I)+AUX(9,I)
210      DELT=DELT+DELT
211      Y(I)=AUX(1,I)+.3555553333333333D0*H*(AUX(8,I)+DELT+AUX(10,I))
212      GUID 25
213
214      C
215
216      29  DO 30 I=1,NDIM
217      DELT=AUX(9,I)+AUX(10,I)
218      DELT=DELT+DELT+DELT
219      Y(I)=AUX(1,I)+.575D0*H*(AUX(8,I)+DELT+AUX(11,I))
220      GUID 25
221
222      C
223
224      100  THE FOLLOWING PART OF SUBROUTINE DHPCG COMPUTES BY MEANS OF
225      RUNGE-KUTTA METHOD STARTING VALUES FOR THE NOT SELF-STARTING
226      PREDICTOR-CORRECTOR METHOD.
227      DO 101 I=1,NDIM
228      Z=H*AUX(N+7,I)
229      AUX(5,I)=Z
230      Y(I)=AUX(N,I)+4D0*Z
231      Z IS AN AUXILIARY STORAGE LOCATION

```



```

226 C      Z=X+.4D0*H
227      CALL FCI(Z,Y,DERY)
228      DO 102 I=1,NDIM
229      Z=H*DERY(I)
230      AUX(6,I)=Z
231      102 Y(I)=AUX(N,I)+.2969776092477536000*AUX(5,I)+.15875964497103583D0*Z
232 C
233      Z=X+.45573725421878943D0*H
234      CALL FCI(Z,Y,DERY)
235      DO 103 I=1,NDIM
236      Z=H*DERY(I)
237      AUX(7,I)=Z
238      103 Y(I)=AUX(N,I)+.21810038822592047D0*AUX(5,I)-3.0509651486929308D0*
239      1AUX(6,I)+3.8328647604670103D0*Z
240 C
241      Z=X+H
242      CALL FCI(Z,Y,DERY)
243      DO 104 I=1,NDIM
244      Y(I)=AUX(N,I)+.17476028226269037D0*AUX(5,I)-.55148066287873294D0*
245      1AUX(6,I)+1.205335599396523500*AUX(7,I)+.17118478121951903D0*
246      2H*DERY(I)
247      GO TO(9,13,15,21),ISW
248 C
249 C      POSSIBLE BREAK-POINT FOR LINKAGE
250 C
251 C      STARTING VALUES ARE COMPUTED.
252 C      NOW START HAMMING'S MODIFIED PREDICTOR-CORRECTOR METHOD.
253 C      1STEP=3
254      200 IF(N-8)204,202,204
255      201 IF(N-8)204,202,204
256 C
257 C      N=H CAUSES THE RUNS OF AUX TO CHANGE THEIR STORAGE LOCATIONS
258      DO 203 N=2,7
259      DO 203 I=1,NDIM
260      AUX(N-1,I)=AUX(N,I)
261      AUX(N+6,I)=AUX(N+7,I)
262      N=7
263 C
264 C      N LESS THAN 8 CAUSES N+1 TO GET N
265      204 N=N+1
266 C
267 C      COMPUTATION OF NEXT VECTOR Y
268      DO 205 I=1,NDIM
269      AUX(N-1,I)=Y(I)
270      AUX(N+6,I)=DERY(I)
271

```



```

316 18STEP=0
317 DO 221 I=1,NDIM
318 AUX(N-1,I)=AUX(N-2,I)
319 AUX(N-2,I)=AUX(N-4,I)
320 AUX(N-3,I)=AUX(N-6,I)
321 AUX(N+6,I)=AUX(N+5,I)
322 AUX(N+5,I)=AUX(N+3,I)
323 AUX(N+4,I)=AUX(N+1,I)
324 DELT=AUX(N+6,I)+AUX(N+5,I)
325 DELT=DELT+DELT
326 AUX(16,I)=8.962962962962963D0*(Y(I)-AUX(N-3,I))
327 1-3.361111111111111D0*(DERY(I)+DELT+AUX(N+4,I))
328 GO TO 201
329
330
331 H MUST BE HALVED
332 222 IHLF=IHLF+1
333 IF(IHLF-20)223,223,210
334 223 H=.5D0*H
335 18STEP=0
336 DO 224 I=1,NDIM
337 OY(I)=390625D-2*(8.D1*AUX(N-1,I)+135.D0*AUX(N-2,I)+4.D1*AUX(N-3,I)
338 1+AUX(N-4,I))-1171875D0*(AUX(N+6,I)-6.D0*AUX(N+5,I)-AUX(N+4,I))*H
339 0AUX(N-4,I)=.390625D-2*(12.D0*AUX(N-1,I)+135.D0*AUX(N-2,I)+
340 210H.D0*AUX(N-3,I)+AUX(N-4,I))-0234375D0*(AUX(N+6,I)+
341 218.D0*AUX(N+5,I))-9.D0*AUX(N+4,I))*H
342 AUX(N-3,I)=AUX(N-2,I)
343 AUX(N+4,I)=AUX(N+5,I)
344 X=X-H
345 DELT=X-(H+H)
346 CALL FC(DELT,Y,DERY)
347 DO 225 I=1,NDIM
348 AUX(N-2,I)=Y(I)
349 AUX(N+5,I)=DERY(I)
350 Y(I)=AUX(N-4,I)
351 DELT=DELT-(H+H)
352 CALL FC(DELT,Y,DERY)
353 DO 226 I=1,NDIM
354 DELT=AUX(N+5,I)+AUX(N+4,I)
355 DELT=DELT+DELT
356 0AUX(16,I)=8.962962962962963D0*(AUX(N-1,I)-Y(I))
357 1-3.361111111111111D0*(AUX(N+6,I)+DELT+DERY(I))
358 226 AUX(N+5,I)=DERY(I)
359 GO TO 206
360 END

```

```

DHC63200
DHC63210
DHC63220
DHC63230
DHC63240
DHC63250
DHC63260
DHC63270
DHC63280
DHC63290
DHC63300
DHC63310
DHC63320
DHC63330
DHC63340
DHC63350
DHC63360
DHC63370
DHC63380
DHC63390
DHC63400
DHC63410
DHC63420
DHC63430
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DHC63460
DHC63470
DHC63480
DHC63490
DHC63500
DHC63510
DHC63520
DHC63530
DHC63540
DHC63550
DHC63560
DHC63570
DHC63580
DHC63590
DHC63600
DHC63610
DHC63620
DHC63630
DHC63640

```



```

1  SUBROUTINE DREBS(DFN,Y,T,N,JM,IND,JSTART,H,MHMIN,EPS,R,S,MK,IER)
2  C-----D-----LIBRARY 1-----
3  C-----D-----
4  C-----D-----
5  C-----D-----
6  C-----D-----
7  C-----D-----
8  C-----D-----
9  C-----D-----
10 C-----D-----
11 C-----D-----
12 C-----D-----
13 C-----D-----
14 C-----D-----
15 C-----D-----
16 C-----D-----
17 C-----D-----
18 C-----D-----
19 C-----D-----
20 C-----D-----
21 C-----D-----
22 C-----D-----
23 C-----D-----
24 C-----D-----
25 C-----D-----
26 C-----D-----
27 C-----D-----
28 C-----D-----
29 C-----D-----
30 C-----D-----
31 C-----D-----
32 C-----D-----
33 C-----D-----
34 C-----D-----
35 C-----D-----
36 C-----D-----
37 C-----D-----
38 C-----D-----
39 C-----D-----
40 C-----D-----
41 C-----D-----
42 C-----D-----
43 C-----D-----
44 C-----D-----
45 C-----D-----

```

FUNCTION - FIRST ORDER DIFFERENTIAL EQUATION SOLVER -  
 THE METHOD OF BULIRSCH - STOKER FOR  
 DY/DX = F(Y,T)

USAGE - CALL DREBS(DFN,Y,T,N,JM,IND,JSTART,H,MHMIN,  
 EPS,R,S,MK,IER)

PARAMETERS DFN - USER SUPPLIED EXTERNAL SUBROUTINE,  
 F(Y,T,N,DY). DFN MUST CALCULATE DY(1) =  
 F(Y(1),Y(2),Y(3),Y(4),Y(5),Y(6),Y(7),Y(8),Y(9),Y(10))  
 Y - ON INPUT Y(1),Y(2),Y(3),Y(4),Y(5),Y(6),Y(7),Y(8),Y(9),Y(10) ARE INITIAL VALUES  
 ON OUTPUT Y(1),Y(2),Y(3),Y(4),Y(5),Y(6),Y(7),Y(8),Y(9),Y(10) CONTAIN AN  
 APPROXIMATE SOLUTION TO Y AT T (AS SET ON  
 OUTPUT)

T - T IS THE INDEPENDENT VARIABLE. ON INPUT, T  
 SHOULD CONTAIN THE INITIAL VALUE OF THE  
 INDEPENDENT VARIABLE. ON OUTPUT, T  
 CONTAINS THE UPDATED VALUE OF THE INDEPENDENT  
 VARIABLE.

N - THE NUMBER OF EQUATIONS IN THE SYSTEM  
 JM - THE MAXIMUM ORDER OF THE RATIONAL APPROX-  
 IMATION. JM MUST BE LESS THAN 7.

IND - CONVERGENCE TYPE INDICATOR (INPUT)  
 IND = 1 SPECIFIES THE STANDARD ERROR TEST  
 IND = 2 SPECIFIES THE RELATIVE ERROR TEST  
 IND = 3 SPECIFIES THE ABSOLUTE ERROR TEST

JSTART - AN INPUT INDICATOR WITH THE FOLLOWING MEANINGS  
 0 - PERFORM A STEP. THE FIRST STEP  
 MUST BE DONE WITH THIS VALUE OF JSTART SO  
 THAT THE SUBROUTINE CAN INITIALIZE ITSELF.  
 -1 - REPEAT THE LAST STEP WITH A NEW VALUE  
 OF H OR JM. SET TO THE INITIAL VALUES OF Y, S,  
 AND T FROM THE MOST RECENT CALL TO  
 DREBS WITH JSTART = 0.

H - ON INPUT, H IS AN INITIAL GUESS FOR THE STEP  
 SIZE.  
 ON OUTPUT, H CONTAINS A SUGGESTED STEP SIZE  
 FOR THE NEXT STEP. THE SUGGESTED VALUE MAY  
 BE LARGER OR SMALLER THAN THE ORIGINAL  
 STEP SIZE.

MHMIN - MHMIN IS THE SMALLEST PERMISSIBLE STEP SIZE.  
 DREBS WILL DECREASE THE STEP SIZE.





```

91  N7=N6+N5+N3
92  N8=N7+N5+N3
93  N2P1=V2+1
94  N3P1=V3+1
95  N8P1=V8+1
96  IF(JV.GT.0.AND.JM.LE.6) GO TO 5
97  IER=66
98  JM=6
99  C C C C
100  S JMAX = JM+4
101  IF(JSTART.NE.0) GO TO 135
102  C C C C
103  TOLD = T
104  IJK4=N4
105  DO 10 I = 1,N
106  AK(I) = Y(I)
107  IJK4=IJK4+1
108  AK(IJK4) = S(I)
109  10 CONTINUE
110  C C C C
111  CALL OFN(Y,I,N,WK(N3P1))
112  C C C C
113  15 BH = .FALSE.
114  KUNVF = .TRUE.
115  20 A = H+T
116  BU = .FALSE.
117  C C C C
118  C C C C
119  C C C C
120  C C C C
121  C C C C
122  C C C C
123  C C C C
124  C C C C
125  C C C C
126  C C C C
127  C C C C
128  C C C C
129  C C C C
130  C C C C
131  C C C C
132  C C C C
133  C C C C
134  C C C C
135  C C C C

```

```

DIRB0920
DIRB0930
DIRB0940
DIRB0950
DIRB0960
DIRB0970
DIRB0980
DIRB0990
DIRB1000
DIRB1010
DIRB1020
DIRB1030
DIRB1040
DIRB1050
DIRB1060
DIRB1070
DIRB1080
DIRB1090
DIRB1100
DIRB1110
DIRB1120
DIRB1130
DIRB1140
DIRB1150
DIRB1160
DIRB1170
DIRB1180
DIRB1190
DIRB1200
DIRB1210
DIRB1220
DIRB1230
DIRB1240
DIRB1250
DIRB1260
DIRB1270
DIRB1280
DIRB1290
DIRB1300
DIRB1310
DIRB1320
DIRB1330
DIRB1340
DIRB1350
DIRB1360

```

FOR AN EXTRAPOLATION OF ORDER JM,  
JM+1 APPROXIMATIONS ARE REQUIRED.  
THREE MORE ARE ALLOWED IN ATTEMPTING  
TO ACHIEVE CONVERGENCE.

INITIALIZATION  
SAVE THE INITIAL VALUES FOR THE DEP-  
ENDENT VARIABLES AND THE ERROR TEST  
VECTOR FOR THE STEP

USE THE FUNCTION ROUTINE TO OBTAIN  
THE INITIAL SLOPES  
DZ = DY/DX

THE LOGICAL VARIABLE, BH, DETERMINES  
WHETHER THE STEP SIZE HAS BEEN  
HALVED, INITIALLY FALSE.  
LATER, BH IS FALSE IF THE STEP SIZE IS  
CUT BY A FACTOR NUT 2

PRESET THE CONVERGENCE SUCCESS FLAG  
TRUE

ADVANCE THE INDEPENDENT VARIABLE BY  
THE STEP SIZE, H

SET THE SWITCH NO FOR THE FIRST SET  
OF COEFFICIENTS, D

INITIALIZE THE H SEQUENCE...

```

136 C
137
138
139 CC
140 CC
141 CC
142 CC
143 C
144 C
145 C
146 C
147 C
148 C
149 C
150 C
151 CC
152 CC
153 CC
154 CC
155 CC
156 CC
157 CC
158 CC
159 CC
160 CC
161 CC
162 CC
163 CC
164 CC
165 CC
166 CC
167 CC
168 CC
169 CC
170 CC
171 CC
172 CC
173 CC
174 CC
175 CC
176 CC
177 CC
178 CC
179 CC
180 CC

M = 1
JR = 2
JS = 3

JJ = 0

IJ6 = N6 - N
IJ7 = N7 - N
I6 = IJ6
I7 = IJ7
DO 125 J = 1, JMAX

      IJ6 = IJ6 + N
      IJ7 = IJ7 + N
      IF (.NOT. BO) GO TO 25
      D(2) = 1.7777777777778D0
      D(4) = 1.1111111111111D0
      D(6) = 28.4444444444444D0
      GO TO 30
      D(2) = 2.25D0
      D(4) = 9.0D0
      D(6) = 36.0D0

      25

      KVV = .TRUE.
      IF (J.LE. (JM/2)) KVV = .FALSE.
      IF (J.LE. (JM+1)) GO TO 30

      L = JM+1
      D(L) = 4.0D0 * D(L-2)

      30

      FC = .7071068 * FC
      GO TO 40

```

```

H/M,H/JR,H/JS

JJ IS THE INDEX FOR THE ARRAY OF
VALUES SAVED IN CASE THE INTERVAL
MUST BE HALVED

INTEGRATION STEP
MIDPOINT + EXTRAPOLATION

SET THE VALUES OF THE EXTRAPOLATION
COEFFICIENTS TO THEIR CORRECT VALUES
FOR THIS EXTRAPOLATION STEP

IF THE ORDER OF THE EXTRAPOLATION
STEP BEING COMPUTED IS LESS THAN JM/2
SET KVV FALSE

RESTRICT THE ORDER OF THE EXTRAPOL-
ATION TO JM
ADJUST THE EXTRAPOLATION COEFFICIENT

DISCOURAGE THE STEP-INCREASING FACTOR
FC, BY A FACTOR OF SQR(2) SINCE
CONVERGENCE WAS NOT OBTAINED
IN JM EXTRAPOLATIONS

```

```

DIRH1370
DIRH1380
DIRH1390
DIRH1400
DIRH1410
DIRH1420
DIRH1430
DIRH1440
DIRH1450
DIRH1460
DIRH1470
DIRH1480
DIRH1490
DIRH1500
DIRH1510
DIRH1520
DIRH1530
DIRH1540
DIRH1550
DIRH1560
DIRH1570
DIRH1580
DIRH1590
DIRH1600
DIRH1610
DIRH1620
DIRH1630
DIRH1640
DIRH1650
DIRH1660
DIRH1670
DIRH1680
DIRH1690
DIRH1700
DIRH1710
DIRH1720
DIRH1730
DIRH1740
DIRH1750
DIRH1760
DIRH1770
DIRH1780
DIRH1790
DIRH1800
DIRH1810
DIRH1820
DIRH1830
DIRH1840
DIRH1850
DIRH1860
DIRH1870
DIRH1880

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181 CCCCCC
182
183
184
185
186
187
188
189
190 C C C
191
192
193
194
195
196 C C C C C
197
198
199
200
201 C C
202
203
204
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206
207
208
209
210
211
212
213
214
215
216
217 C
218
219
220
221
222
223
224
225

35 L = J
   U(L) = DFLOAT(M*M)
   FC = 1.0+FLOAT(JM+1-J)*.1666667
      IF THE NUMBER, J, OF EXTRAPOLATIONS HAS
      NOT EXCEEDED JM
      FIND U(J) = ((H DIVIDED BY H/M)**2
      ADJUST THE FACTOR, FC, USED TO ADJUST
      THE STEPSIZE FOR THE NEXT STEP TO BE
      TAKEN

40 M = M+M
   G = H/FLOAT(M)
   B = G+G
      MODIFIED MIDPOINT RULE USED TO FIND
      FIRST VALUE FOR THIS EXTRAPOLATION
      STEP

45 IF ((.NOT. BH) .OR. (J .GE. (JMAX-1))) GO TO 50
      IF THE STEPSIZE HAS NOT BEEN HALVED
      OR IF THE ORDER OF THE EXTRAPOLATION
      STEP EXCEEDS THAT FOR WHICH PREVIOUS-
      LY COMPUTED VALUES WERE SAVED, THEY
      MUST BE COMPUTED
      (JMAX-1) GO TO 50
      OTHERWISE THE VALUES HAVE BEEN SAVED
      AND CAN BE RESTORED

50 IJK1=N
   IJK2=N2
   IJK6=IJK6
   IJK7=IJK7
   DO 45 I = 1, N
      IJK2=IJK2+1
      IJK7=IJK7+1
      WK(IJK2) = WK(IJK7)
      IJK1=IJK1+1
      IJK6=IJK6+1
      WK(IJK1) = WK(IJK6)
   CONTINUE
   GO TO 75

45 IJK1=N
   IJK2=N2
   IJK3=N3
   DO 55 I = 1, N
      IJK1=IJK1+1
      WK(IJK1) = WK(I)
      IJK2=IJK2+1

```

```

2267 IJK3=IJK3+1
2270 WK(IJK2) = WK(I)+G*WK(IJK3)
2271 CONTINUE
2272 KH = W/2
2273 XU=1
2274
2275 DO 70 K = 2,M
2276 XU = XU + G
2277 CALL OFN(WK(N2P1),XU,N,WK(NBP1))
2278 IJK1=N
2279 IJK2=N2
2280 IJK8=N8
2281 DO 60 I = 1,N
2282 IJK1=IJK1+1
2283 IJK8=IJK8+1
2284 U = WK(IJK1) + B*WK(IJK8)
2285 IJK2=IJK2+1
2286 WK(IJK1) = WK(IJK2)
2287 WK(IJK2) = U
2288 CONTINUE
2289
2290 IF ((K .NE. KH) .OR. (K .EQ. 3)) GO TO 70
2291 JJ = 1+JJ
2292 I6=I6+N
2293 I7=I7+N
2294 IJK1=N
2295 IJK2=N2
2296 IJK6=I6
2297 IJK7=I7
2298 DO 65 I = 1,N
2299 IJK2=IJK2+1
2300 IJK7=IJK7+1
2301 WK(IJK7) = WK(IJK2)
2302 IJK6=IJK6+1
2303 IJK1=IJK1+1
2304 WK(IJK6) = WK(IJK1)
2305 CONTINUE
2306 CONTINUE
2307 CALL OFN(WK(N2P1),A,N,WK(NBP1))
2308
2309 CCCCC
2310
2311 CCCCC
2312
2313 CCCCC
2314
2315 CCCCC
2316
2317 CCCCC
2318
2319 CCCCC
2320
2321 CCCCC
2322
2323 CCCCC
2324
2325 CCCCC
2326
2327 CCCCC
2328
2329 CCCCC
2330
2331 CCCCC
2332
2333 CCCCC
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2335 CCCCC
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2337 CCCCC
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2341 CCCCC
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2357 CCCCC
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2363 CCCCC
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2367 CCCCC
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2369 CCCCC
2370

```

THE MEMBER OF THE H SEQUENCE  
BEING USED BY THE MIDPOINT INTEGRA-  
TION RULE IS H/M. COMPUTE THE END  
OF THE STEP FOR EACH DEPENDENT VARI-  
ABLE

IN CASE THE INTERVAL MUST BE HALVED  
NEXT TIME, SAVE THE VALUES AT HALF MAY  
ALONG (KH=W/2) THE STEP UNLESS KE3  
GO TO 70



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271 C C C C C
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306
307
308
309
310
311
312
313
314
315

IJK1=N
IJK2=N2
IJK5=N5
IJK8=N8
DO 115 I = 1,N

      V IS USED TO SAVE THE VALUE OBTAINED
      BY THE MIDPOINT RULE USING THE PREVI-
      OUS MEMBER OF THE H SEQUENCE
      (THE FIRST TIME THROUGH THIS VALUE IS
      MEANINGLESS, BUT IT IS NOT USED SINCE
      L IS LESS THAN 2)

      IJK1=IJK1+1
      IJK2=IJK2+1
      IJK5=IJK5+1
      IJK8=IJK8+1
      IF (L .GE. 2) V = WK(IJK5)
      COMPUTE THE FINAL VALUE OBTAINED FOR
      THIS MEMBER OF THE H SEQUENCE BY THE
      MODIFIED MIDPOINT RULE

      IJK8=IJK8+1
      WK(IJK5) = (WK(IJK2) + WK(IJK1))*.5HALF
      C = WK(IJK5)
      I A = C

      IF (L .LT. 2) GO TO 90

      AT LEAST TWO VALUES ARE NEEDED TO
      START EXTRAPOLATION

      IF THE VALUE JUST COMPUTED BY THE
      MIDPOINT RULE SHOWS A LARGE JUMP FROM
      THE PREVIOUS, HALVE THE INTERVAL
      DABS(C)) .AND. (H .NE. HMIN) .AND.
      DO 130
      PERFORM THE L STEPS FOR THE CURRENT
      LTH ORDER EXTRAPOLATION STEP. IF THE
      DENOMINATOR OF THE RATIONAL FUNCTION
      GOES TO ZERO AT ANY STEP, SET IT AT
      THAT STEP TO ITS VALUE JUST BEFORE

      IP5=IJK5
      DO 85 K = 2,L
      IP5=IP5+V
      H1 = D(K) * V
      H = H1-C
      U = V
      IF (H .EQ. 0.) GO TO 80
      H = (C-V)/H

```



```

316      U = C*H
317      C = H1*H
318      IF(K-LI-L) V=WK(IP5)
319      WK(IP5) = U
320      FA = U + 1A
321      CONTINUE
322
323      GO TO (95,100,105),IND
324
325      UST=DABS(1A)
326      IF(UST.GT.S(I)) S(I)=UST
327      GO TO 110
328      S(I)=DABS(Y(I))
329      GO TO 110
330      S(I)=1
331      R(I)=DABS(Y(I)-1A)
332      Y(I)=1A
333      IF(S(I).LT.EPS) S(I)=EPS
334      IF(R(I).GT.EPS*S(I)) KONV=.FALSE.
335      CONTINUE
336      IF(KONV) GO TO 155
337
338      D(3) = 4.
339      D(5) = 16.
340
341      BU = (.NOT.BU)
342      IJK4=N4
343      DO 120 J=1,N
344      IJK4=IJK4+1
345      S(I)=WK(IJK4)
346      CONTINUE
347
348      V = JR
349      JR = JS
350      JS = V+M
351
352      125 CONTINUE
353
354      IF, AFTER ALL THE EXTRAPOLATIONS
355      ALLOWED, CONVERGENCE HAS NOT BEEN
356      ACHIEVED, ATTEMPT TO HALVE H SO THAT

```

USE THE ERROR ROUTINE FOR EACH  
DEPENDENT VARIABLE TO CHECK WHETHER  
CONVERGENCE HAS BEEN ACHIEVED

RESET THE EXTRAPOLATION COEFFICIENTS

FLIP THE BU SWITCH FOR THE NEXT SET  
OF COEFFICIENTS

RESET S

TAKE THE NEXT MEMBER  
OF THE H SEQUENCE

AND GO BACK FOR THE  
NEXT EXTRAPOLATION

IF, AFTER ALL THE EXTRAPOLATIONS  
ALLOWED, CONVERGENCE HAS NOT BEEN  
ACHIEVED, ATTEMPT TO HALVE H SO THAT

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THE SAVED VALUES CAN BE USED (SET BH
TRUE FOR THIS PURPOSE)
IF HALVING H MAKES IT LESS THAN HMIN,
SET H = HMIN
IN THIS CASE THE SAVED VALUES CANNOT
BE USED
IF H HAD ALREADY BEEN AT HMIN,
CONVERGENCE CANNOT BE ACHIEVED FOR
THIS HMIN AND THIS EPS CRITERION.
SET KUNV FALSE

      HH = (.NOT. BH)
      IF (DABS(H) .LE. DABS(HMIN)) GO TO 150
      H = H * HALF
      IF (DABS(H) .GE. DABS(HMIN)) GO TO 20
      H = DSIGN(HMIN,H)
      GO TO 15
135 DO 140 I = 1,N
      DO 140 Y(I) = WK(I)
140 CONTINUE
      IJK4=V4
      DO 145 I=1,N
      IJK4=IJK4+1
      S(I)=WK(IJK4)
145 CONTINUE
      I = IJLD
      GO TO 15
150 KUNV = .FALSE.

      IF (KUNV) GO TO 160
      IER=129
      IF (IER.EQ.0) GO TO 9005
      GO TO 9000
      CALL JERIST (IER,6HDREBS )
      GO TO 9005
      RETURN
      END

```



```

1  SUBROUTINE DVOGER(Y,T,N,MTH,MAXDER,JSTART,H,HMIN,HMAX,EPS,
2  YMAX,ERROR,WK,IER)
3  C-----LIBRARY I-----
4  C-----D-----
5  C-----
6  C-----
7  C-----
8  C-----
9  C-----
10 C-----
11 C-----
12 C-----
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38 C-----
39 C-----
40 C-----
41 C-----
42 C-----
43 C-----
44 C-----
45 C-----

```

FUNCTION  
 USAGE  
 PARAMETERS DFUN

- FIRST ORDER DIFFERENTIAL EQUATION SOLVER-  
 GEAR'S METHOD FOR  $dx/dt = f(x,t)$   
 - CALL DVOGER(DFUN,Y,I,N,MTH,MAXDER,JSTART,H,  
 HMIN,HMAX,EPS,YMAX,ERROR,WK,IER)  
 - USER SUPPLIED EXTERNAL SUBROUTINE, DFUN(YP,TP,  
 M,DY,PW,IND), WHERE  
 YP CONTAINS THE PRESENT (I.E. AT TP)  
 SOLUTION VECTOR AS  $x(1)=YP(1,1)$ ,  
 $x(2)=YP(1,2), \dots, x(N)=YP(1,N)$ ,  
 TP IS THE PRESENT TIME, AND  
 M IS THE ORDER OF THE JACOBIAN.  
 IF IND=0, DFUN MUST COMPUTE THE N-VECTOR  
 $f(YP,TP)$  AND STORE THE VALUES IN DY.  
 IF IND=1, DFUN MUST COMPUTE THE JACOBIAN OF  
 $f$  EVALUATED AT  $(YP,TP)$  AND STORE THE  
 RESULT IN THE M BY M MATRIX PW.  
 THE JACOBIAN IS COMPUTED ONLY FOR CALLS WITH  
 MTH=1.  
 YP IS AN 8 BY N ARRAY. THE SOLUTION COMPONENTS  
 ARE  $Y(1,1), Y(1,2), \dots, Y(1,N)$ .  
 Y IS A TWO DIMENSIONAL ARRAY (8 BY N)  
 CONTAINING THE DEPENDENT VARIABLES AND THEIR  
 SCALED DERIVATIVES. THE SOLUTION COMPONENTS  
 ARE  $x(1) = Y(1,1), x(2) = Y(1,2), \dots$ , THE J-TH  
 $x(N) = Y(1,N)$  AND  $Y(J+1,1)$  CONTAINS THE J-TH  
 DERIVATIVE OF  $x(1)$  SCALED BY  $H \cdot J!$  FACTORIAL  
 (J). HERE H IS THE CURRENT STEP SIZE.  
 ONLY  $Y(1,1), I=1,2, \dots, N$  NEED BE PROVIDED BY  
 THE CALLING PROGRAM ON THE FIRST CALL TO  
 DVOGER, WITH JSTART=0.  
 T IS THE INDEPENDENT VARIABLE. ON INPUT, T  
 SHOULD CONTAIN THE INITIAL VALUE OF THE  
 INDEPENDENT VARIABLE. ON OUTPUT, T  
 CONTAINS THE UPDATED VALUE OF THE INDEPEN-  
 DENT VARIABLE.  
 N IS THE NUMBER OF FIRST ORDER DIFFERENTIAL  
 EQUATIONS.  
 MTH IS THE METHOD INDICATOR. THE USER MAY  
 SELECT ONE OF THE FOLLOWING.  
 MTH=0 INDICATES A PREDICTOR-CORRECTOR  
 (ADAMS) METHOD









```

      DATA  

      *  

      *  

      *  

      *  

      *  

      JER=0  

      JER=0  

      N4=N*N*(EQ-0) N4=0  

      IF(MTH.EQ.0) N4=0  

      N1=N+10+N4  

      N2 = V1 + 1  

      N3 = N  

      N5 = N1 + N  

      N6 = N5 + 1  

      N7=N6+N+N  

      N8=N7+N  

      N9=N8+N  

      N10=N8-1  

      IND1=V4+1  

      IND2=N4+2  

      IND9=V4+9  

      IND10=N4+10  

      IRET = 1  

      KFLAG = 1  
  

      MXDER=MAXDER  

      IF(MTH.EQ.0) GO TO 5  

      IF(MAXDER.LE.6) GO TO 10  

      JER=68  

      MAXDER=6  

      GO TO 10  

      IF(MAXDER.LE.7) GO TO 10  

      JER=68  

      MAXDER=7  

      S

```

ERROR,RACUM,WK,X,K,ZERO,HALF,ONE,UNEP

DABS,DMAXI,DMINI

C(2),ZERO,HALF,ONE,ONEP,NDIG/-1.D0,0.00,..5D0,

1.D0,1.0000

CUEFF CONAINS THE COEFFICIENTS

USED IN SELECTING THE STEP SIZE AND

THE ORDER OF THESE CONSTANTS NEED ONLY

BE ACCURATE TO A FEW DIGITS.

COEF/2.0,45.7,33.10,42.13,7.17,15.1,,

2.0,12.0,24.0,37.89,53.33,70.08,87.97,

3.0,6.0,9.16,12.5,15.98,1.0,1.0,

12.0,24.0,37.89,53.33,70.08,87.97,1.0,

1.1,0.5,0.1667,0.04133,0.008267,1.0,

1.0,1.0,2.0,1.0,.3157,.07407,.0136,

DVUG1380

DVUG1390

DVUG1420

DVUG1430

DVUG1440

DVUG1450

DVUG1460

DVUG1470

DVUG1480

DVUG1490

DVUG1500

DVUG1510

DVUG1520

DVUG1530

DVUG1540

DVUG1550

DVUG1560

DVUG1570

DVUG1580

DVUG1590

DVUG1600

DVUG1610

DVUG1620

DVUG1630

DVUG1640

DVUG1650

DVUG1660

DVUG1670

DVUG1680

DVUG1690

DVUG1700

DVUG1710

DVUG1720

DVUG1730

DVUG1740

DVUG1750

DVUG1760

DVUG1770

DVUG1780

DVUG1790

DVUG1800

DVUG1810

DVUG1820

DATA

\* \*

\* \*

\* \*

JER=0

JER=0

N4=N\*N\*(EQ-0) N4=0

IF(MTH.EQ.0) N4=0

N1=N+10+N4

N2 = V1 + 1

N3 = N

N5 = N1 + N

N6 = N5 + 1

N7=N6+N+N

N8=N7+N

N9=N8+N

N10=N8-1

IND1=V4+1

IND2=N4+2

IND9=V4+9

IND10=N4+10

IRET = 1

KFLAG = 1

MXDER=MAXDER

IF(MTH.EQ.0) GO TO 5

IF(MAXDER.LE.6) GO TO 10

JER=68

MAXDER=6

GO TO 10

IF(MAXDER.LE.7) GO TO 10

JER=68

MAXDER=7

S

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10 IF (JSTART .LE. 0) GO TO 35

15 DO 20 I = 1,N
   DO 20 J = 1,K
     WK(N4+J,I)=Y(J,I)
20 CONTINUE
   HNEW = HNEW HOLD) GO TO 30
25 IF (H .EQ. HOLD) GO TO 30
   RACUM = H/HOLD
   IRET1 = 1
   GO TO 375
30 IOLD = I
   TOLD = T
   RACUM = ONE
   IF (JSTART .GT. 0) GO TO 135
   GO TO 50
35 IF (JSTART .EQ. -1) GO TO .45

10 = 1
CALL DFUN(Y,T,N,WK(N2,1),WK,0)
DO 40 I = 1,N
   N11 = N1 + I
   Y(2,I)=WK(N11,1)*H
40 CONTINUE
   HNEW = H
   K = 2
   GO TO 15

45 IF (I) .EQ. IOLD) JSTART = 1
   I = IOLD
   IO = IOLD
   K = IJ + 1
   GO TO 25

50 IF (WH .EQ. 0) GO TO 55
   GO TO (95,100,105,110,115,120),IO
55 GO TO (60,65,70,75,80,85,90),IO
60 C(1) = -ONE

```

TAKE A STEP CONTINUING FROM THE LAST  
 STEP. SAVE INFORMATION FOR A POSSIBLE  
 RESTART AND CHECK H FOR A POSSIBLE  
 USER CHANGE. HNEW IS THE PREVIOUS  
 STEP SIZE AND IO IS THE CURRENT UNDER

FIRST CALL, THE ORDER IS SET TO 1 AND  
 THE INITIAL DERIVATIVES CALCULATED.

REPEAT LAST STEP. RESTORE THE SAVED  
 INFORMATION.

SET ALL COEFFICIENTS DETERMINED BY  
 THE ORDER AND THE METHOD TYPE.

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 DVUG1930  
 DVUG1940  
 DVUG1950  
 DVUG1960  
 DVUG1970  
 DVUG1980  
 DVUG1990  
 DVUG2000  
 DVUG2010  
 DVUG2020  
 DVUG2030  
 DVUG2040  
 DVUG2050  
 DVUG2060  
 DVUG2070  
 DVUG2080  
 DVUG2090  
 DVUG2100  
 DVUG2110  
 DVUG2120  
 DVUG2130  
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 DVUG2240  
 DVUG2250  
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DVUG22H0  
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DVUG2990  
DVUG3000  
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110

GO 10 125  
C(1)=-HALF  
C(3)=-HALF  
GO 10 125  
C(1)=-0.4166666666666667D0  
C(3)=-0.75D0  
C(4)=-0.1666666666666667D0  
GO 10 125  
C(1)=-0.375D0  
C(3)=-0.9166666666666667D0  
C(4)=-0.3333333333333333D0  
C(5)=-0.0416666666666667D0  
GO 10 125  
C(1)=-0.3486111111111111D0  
C(3)=-1.0416666666666667D0  
C(4)=-0.4861111111111111D0  
C(5)=-0.1041666666666667D0  
C(6)=-0.008333333333333333D0  
GO 10 125  
C(1)=-0.3298611111111111D0  
C(3)=-1.1416666666666667D0  
C(4)=-0.625D0  
C(5)=-0.1770833333333333D0  
C(6)=-0.025D0  
C(7)=-0.00138888888888889D0  
GO 10 125  
C(1)=-0.3155919312169312D0  
C(3)=-1.225D0  
C(4)=-0.7518518518518519D0  
C(5)=-0.2552083333333333D0  
C(6)=-0.0486111111111111D0  
C(7)=-0.4861111111111111D0-2  
C(8)=-1.984126984126984D-3  
GO 10 125  
C(1)=-ONE  
C(3)=-ONE  
GO 10 125  
C(1)=-0.6666666666666667D0  
C(3)=-0.3333333333333333D0  
GO 10 125  
C(1)=-0.5454545454545455D0  
C(3)=-0.090909090909091D0  
C(4)=-0.090909090909091D0  
GO 10 125  
C(1)=-0.48D0  
C(3)=-0.7D0



DVUG3020  
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IF THE JACOBIAN MUST BE RE-CALCULATED  
 BECAUSE OF AN ORDER CHANGE, SET  
 IWEVAL POSITIVE IF IT HAS NOT YET BEEN  
 DONE (IRET=1) OR SKIP TO A FINAL SCAL-  
 ING IF IT HAS BEEN COMPLETED (IRET=2).  
 IF THE CURRENT ORDER OF ERRORS IN-  
 CREASES THE ORDER, EDWN IS USED TO  
 DECREASE THE ORDER.

C(4) = -0.200  
 C(5) = -0.0200  
 GO TO 125  
 C(1) = -0.43795620437956200  
 C(3) = -0.821167883211678800  
 C(4) = -0.310218978102189800  
 C(5) = -0.0547445255474452600  
 C(6) = -0.003649635036496350400  
 GO TO 125  
 C(1) = -0.408163265306122500  
 C(3) = -0.920634920634920600  
 C(4) = -0.416666666666666700  
 C(5) = -0.099206349206349200  
 C(6) = -0.011904761904761900  
 C(7) = -0.00056689342403628200

K = IO+1  
 IDOUB = (4 - MTH)/2  
 MTYP = HALF/(IO + 1)  
 ENQ2 = HALF/(IO + 2)  
 ENQ3 = HALF/(IO)  
 ENQ1 = EPS  
 PEP SH = EPS  
 EUP = (COEF(IO,MTYP,2)\*PEPSH)\*\*2  
 EDWN = (COEF(IO,MTYP,1)\*PEPSH)\*\*2  
 IF (EDWN.EQ.0) GO TO 390  
 BND = EPS\*ENQ3/N  
 IWEVAL = MTH  
 GO TO (135,340), IRET

COMPUTE THE PREDICTED Y VALUES BY  
 EFFECTIVELY MULTIPLYING THE SAVED  
 INFORMATION BY THE PASCAL TRIANGLE  
 MATRIX.

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CCCC

T = I + H  
 DO 140 J = 2,K



```

316 DO 140 J1 = J1 + J - 1
317 J2 = K
318 DO 140 I = 1, N
319 Y(J2, I) = Y(J2, I) + Y(J2+1, I)
320
321 140 CONTINUE
322
323 CCCCCCCCCC
324
325 TAKE UP TO 3 CORRECTOR ITERATIONS.
326 CONVERGENCE IS TESTED BY REQUIRING
327 CHANGES TO BE LESS THAN BND.
328 THE SUMS OF THE CORRECTIONS ARE
329 ACCUMULATED IN THE ARRAY ERROR(I).
330 IS EQUAL TO THE K-TH DERIVATIVE OF
331 MULTIPLIED BY H**K/(FACTORIAL(K-1)
332 (C(K))). ERROR(I) IS THEREFORE PRO-
333 PORTIONAL TO THE ACTUAL ERRORS IN THE
334 LOWEST POWER OF H PRESENT. (H**K)
335
336 DO 145 I = 1, N
337 ERROR(I) = ZERO
338 CONTINUE
339 DO 220 L = 1, 3
340 CALL DFUN(Y, T, N, WK(N2, 1), WK, 0)
341
342 IF (IMEVAL .LT. 1) GO TO 185
343 IF (MTH.EQ.2) GO TO 165
344 CALL DFUN(Y, T, N3, WK, WK, 1)
345 R = C(1)*H
346 DO 150 I = 1, N4
347 WK(I, 1) = WK(I, 1)*R
348 CONTINUE
349 N11 = N3 + 1
350 N12 = N*N11 - N3
351 DO 160 I = 1, N12, N11
352 WK(I, 1) = WK(I, 1)+ONE
353 CONTINUE
354 IMEVAL = -1
355 IF (N.EQ.1) GO TO 185
356 CALL LUDEIF(WK, WK, N, N3, NDIG, D1, D2, WK(N7, 1), WK(N8, 1), WK(N9, 1),
357 KER)
358 IF (KER) 185, 185, 225
359
360

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DVUG3620
DVUG3630
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DVUG3980
DVUG3990
DVUG4000
DVUG4010
DVUG4020
DVUG4030
DVUG4040
DVUG4050
DVUG4060

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361 DO 170 I = 1,N
362 AK(IND9,I)=Y(1,I)
363 CONTINUE
364 DO 180 J = 1,N
365 R=EPS*DMAX1(EPS,DABS(WK(IND9,J)))
366 Y(1,J)=Y(1,J)+R
367 D=C(1)*H/R
368 CALL DFUN(Y,I,N,WK(N6,1),WK,0)
369 DO 175 I = 1,N
370 N11 = I + (J-1)*N3
371 N12 = N5 + I
372 N13 = N1 + I
373 WK(N11,1)=(WK(N12,1)-WK(N13,1))*D
374 CONTINUE
375 Y(1,J)=WK(IND9,J)
376 CONTINUE
377 GO TO 155
378 IF (M1H.NE.0) GO TO 195
379 DO 190 I = 1,N
380 N11 = N1 + I
381 WK(IND9,I)=Y(2,I)-WK(N11,1)*H
382 CONTINUE
383 GO TO 210
384 DO 200 I = 1,N
385 N11 = N5 + I
386 N12 = N1 + I
387 WK(N11,1)=Y(2,I)-WK(N12,1)*H
388 CONTINUE
389 IF (N8.GT.1) GO TO 202
390 WK(N8,1)=WK(N6,1)/WK(1,1)
391 GO TO 203
392 CALL LUFLMF(WK,WK(N6,1),WK(N7,1),N,N3,WK(N8,1))
393 DO 205 I=1,N
394 WK(IND9,I)=WK(N10+I,1)
395 CONTINUE
396 NT=N
397 DO 215 I = 1,N
398 I=Y(1,I)+C(1)*WK(IND9,I)
399 Y(2,I)=Y(2,I)-WK(IND9,I)
400 ERROR(I)=ERROR(I)+WK(IND9,I)
401 IF (DABS(WK(IND9,I)).LE.(BND*YMAX(I))) NT=NT-1
402 CONTINUE
403 IF (NT.LE.0) GO TO 245
404
405 C

```

THE CORRECTOR FAILED TO CONVERGE IN

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406 CCCCCCCCCC
407
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450

225 I = T - H
    IF ((DABS(H) - LE, (DABS(HMIN)*ONEP)) .AND. ((IWEVAL - M1YP) .LT.
    * IF ((MTH - EQ. 0) .OR. (IWEVAL .NE. 0)) RACUM = RACUM*0.25
    IWEVAL = MTH
    GO TO 375
    IRET1 = 2
    GO TO 375
    KFLAG = -3
    DO 240 I = 1, N
    DO 240 J = 1, K
    Y(J, I) = WK(N4+J, I)
    240 CONTINUE
    H = H*OLD
    IO = IO*OLD
    JSTART = IO
    GO TO 395

ITERATIONS, VARIOUS POSSIBILITIES ARE DVUG4540
CHECKED. IF H IS EQUAL TO HMIN AND DVUG4550
THIS IS THE ADAMS METHOD OR A STIFF DVUG4560
METHOD IN WHICH THE JACOBIAN HAS DVUG4570
ALREADY BEEN RE-EVALUATED. A NO CON- DVUG4580
VERGENCE EXIT IS TAKEN, OTHERWISE THE DVUG4590
JACOBIAN IS RE-EVALUATED AND/OR THE DVUG4600
STEP IS REDUCED TO TRY TO OBTAIN DVUG4610
CONVERGENCE. DVUG4620
DVUG4630
DVUG4640
DVUG4650
DVUG4660
DVUG4670
DVUG4680
DVUG4690
DVUG4700
DVUG4710
DVUG4720
DVUG4730
DVUG4740
DVUG4750
DVUG4760
DVUG4770
DVUG4780
DVUG4790
DVUG4800
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DVUG4860
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DVUG4880
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DVUG4900
DVUG4910
DVUG4920
DVUG4930
DVUG4940
DVUG4950
DVUG4960
DVUG4970
DVUG4980
DVUG4990
DVUG5000

THE CORRECTOR CONVERGED AND CONTROL
IS PASSED TO STATEMENT 260 IF THE
ERROR TEST IS PASSED, AND TO 270
OTHERWISE.
IF THE STEP IS O.K. IT IS ACCEPTED.
IF IDOUB HAS BEEN REDUCED TO ONE,
A TEST IS MADE TO SEE IF THE STEP CAN
BE INCREASED AT ONE LOWER, THE A STEP
CURRENT, IS ONLY MADE IF THE STEP CAN
BE INCREASED BY AT LEAST 1.1*M. IF NO
CHANGE IS POSSIBLE, IDOUB IS SET TO
10 TO PREVENT FURTHER TESTING FOR THE
NEXT TEN STEPS.
IF A CHANGE IS POSSIBLE, IT IS MADE
AND IDOUB IS SET TO 10 TO PREVENT
FURTHER TESTING FOR THAT NUMBER OF
STEPS. IF THE ERROR WAS TOO LARGE,
THE OPTIMUM STEP SIZE FOR THIS OR
SOME LOWER ORDER IS COMPUTED, AND THE

```



```

451 C
452 C
453 C
454 C
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482 C
483 C
484 C
485 C
486 C
487 C
488 C
489 C
490 C
491 C
492 C
493 C
494 C
495 C

245 D = ZERO
250 DO 250 I = 1,N
      O = D + (ERROR(I)/YMAX(I))*2
250 CONTINUE
      IWEVAL = 0
      IF (D.GT. E) GO TO 270
      IF (K.LT. 3) GO TO 260
      DO 255 J = 3,K
        O = 0
        DO 255 I = 1,N
          Y(J,I) = Y(J,I) + C(J)*ERROR(I)
255 CONTINUE
260 KFLAG = +1
      HNEA = H
      IF (IDJUB.LE. 1) GO TO 275
      IDJUB = IDJUB - 1
      IF (IDJUB.GT. 1) GO TO 350
      DO 265 I = 1,N
        WK(IND10,I) = ERROR(I)
265 CONTINUE
      GO TO 350
270 KFLAG = KFLAG - 2
      IF (DABS(H).LE. (DABS(HMIN)*DNEP)) GO TO 370
      I = 1
      IF (KFLAG.LE. -5) GO TO 360
      PR2 = (D/E)*ENQ2*1.2
      PR3 = 1.E+20
      IF ((I).GE. MXDER) .OR. (KFLAG.LE. -1)) GO TO 285
      D = ZERO
      DO 280 I = 1,N
        D = D + ((ERROR(I) - WK(IND10,I))/YMAX(I))*2
280 CONTINUE
      PR3 = (D/EUP)*ENQ3*1.4
285 PR1 = 1.E+20
      IF (IDJUB.LE. 1) GO TO 295
      D = ZERO
      DO 290 I = 1,N
        D = D + (Y(K,I)/YMAX(I))*2
290 CONTINUE
      PR1 = (D/EDWN)*ENQ1*1.3

```

STEP RETRIED. IF IT SHOULD FAIL TWICE  
 MORE IT IS AN INDICATION THAT THE  
 DERIVATIVES THAT HAVE ACCUMULATED IN  
 THE Y ARRAY HAVE ERRORS OF THE WRONG  
 ORDER, SO THE FIRST DERIVATIVES ARE  
 RECOMPUTED AND THE ORDER IS SET TO 1.

DVUG5010  
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 DVUG5110  
 DVUG5120  
 DVUG5130  
 DVUG5140  
 DVUG5150  
 DVUG5160  
 DVUG5170  
 DVUG5180  
 DVUG5190  
 DVUG5200  
 DVUG5210  
 DVUG5220  
 DVUG5230  
 DVUG5240  
 DVUG5250  
 DVUG5260  
 DVUG5270  
 DVUG5280  
 DVUG5300  
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 DVUG5370  
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 DVUG5390  
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 DVUG5460



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DVUG5880  
DVUG5890  
DVUG5900  
DVUG5910  
DVUG5920  
DVUG5930

```

295 CONTINUE
IF (PR2 .LE. PR3) GO TO 325
IF (PR1 .LT. PR3) GO TO 330
R = 1.0/AMAX1(PRI,1.E-4)
300 NEWI = IO
305 IDOUB = 10
IF ((KFLAG.EQ.1) .AND. (R .LT. (1.1))) GO TO 350
IF (NEWI .LE. IO) GO TO 315
XK = JNE / K
DO 310 I = 1, N
310 Y(NEWI+1,I) = ERROR(1)*C(K)*XK
CONTINUE
315 K = NEWI + 1
IF (KFLAG.EQ.1) GO TO 335
RACUM = RACUM*R
IRET1 = 3
GO TO 375
320 IF (NEWI.EQ. IO) GO TO 135
325 IO = NEWI
GO TO 350
IF (PR2 .GT. PR1) GO TO 300
NEWI = IO
K = 1.0/AMAX1(PR2,1.E-4)
GO TO 305
330 K = 1.0/AMAX1(PR3,1.E-4)
NEWI = IO + 1
GO TO 305
335 IRET = 2
H = DMIN1(R,DABS(HMAX/H))
HNEW = H
IF (ID.EQ. NEWI) GO TO 340
IO = NEWI
GO TO 350
340 K1 = JNE
DO 345 J = 2, K
R1 = R1*R
DO 345 I = 1, N
Y(J,I) = Y(J,1)*R1
345 CONTINUE
IDOUB = K
350 DO 355 I = 1, N
YMAX(I) = DMAX1(YMAX(1),DABS(Y(1,I)))
355 CONTINUE
JSTART = IO

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540

```

541 GO TO 395
542 IF (ID.EQ.1) GO TO 390
543 CALL DFUN(Y,I,N,WK(N2,1),WK,0)
544 R = H/HOLD
545 DO 365 I = 1,N
546 Y(I,1) = WK(IND1,1)
547 N11 = N1 + I
548 WK(IND2,1) = HOLD*WK(N11,1)
549 Y(2,1) = WK(IND2,1)*R
550 CONTINUE
551 IO = 1
552 KFLAG = 1
553 GO TO 50
554 KFLAG = -1
555 HNEW = H
556 JSTART = IO
557 GO TO 400
558 C
559 SCALE ALL VARIABLES CONNECTED WITH
560 H AND RETURN TO THE CALLING SECTION
561 RACUM = DMAX1(DABS(HMIN/HOLD),RACUM)
562 R1 = ONE
563 DO 380 J = 2,K
564 R1 = R1*RACUM
565 DO 380 I = 1,N
566 Y(J,I) = WK(N4+J,I)*R1
567 CONTINUE
568 H = HJLD*RACUM
569 DO 385 I = 1,N
570 Y(I,1) = WK(IND1,1)
571 CONTINUE
572 IDUUB = K
573 GO TO (30,135,320),IRET1
574 KFLAG = -4
575 GO TO 235
576 IF(KFLAG.EQ.1) GO TO 9000
577 IER = 32-KFLAG
578 CONTINUE
579 IF(JER.NE.0) CALL UERTST(JER,6HDVDGER)
580 IF(IER.GT.33) IER = IER - 1
581 IF(IER.NE.0) CALL UERTST(IER,6HDVDGER)
582 RETURN
583 END

```

DVUG5940  
 DVUG5950  
 DVUG5960  
 DVUG5970  
 DVUG5980  
 DVUG5990  
 DVUG6000  
 DVUG6010  
 DVUG6020  
 DVUG6030  
 DVUG6040  
 DVUG6050  
 DVUG6060  
 DVUG6070  
 DVUG6080  
 DVUG6090  
 DVUG6100  
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 DVUG6280  
 DVUG6290  
 DVUG6300  
 DVUG6310  
 DVUG6320  
 DVUG6330  
 DVUG6340  
 DVUG6350  
 DVUG6360  
 DVUG6370  
 DVUG6380

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123456789101112131415161718192021222324252627282930313233343536373839404142434445
SUBROUTINE LUDATF (A,LU,N,IA,IOGI,D1,D2,IPVT,EQUIL,WA,IER)
C-----D-----LIBRARY 1-----
FUNCTION
USAGE
PARAMETERS  A
              LU
              N
              IA
              IOGI
              D1
              D2
              IPVT
              EQUIL
              WA
              IER

- L-U DECOMPOSITION BY THE CROUT ALGORITHM
- WITH OPTIONAL ACCURACY TEST.
- CALL LUDATF(A,LU,N,IA,IOGI,D1,D2,IPVT,
  EQUIL,WA,IER)
- INPUT MATRIX OF DIMENSION N BY N CONTAINING
  THE MATRIX TO BE DECOMPOSED
- REAL OUTPUT MATRIX OF DIMENSION N BY N
  CONTAINING THE L-U DECOMPOSITION OF A
  ROWWISE PERMUTATION OF THE INPUT MATRIX.
  FOR A DESCRIPTION OF THE FORMAT OF LU, SEE
  EXAMPLE.
- INPUT SCALAR CONTAINING THE ORDER OF THE
  MATRIX A.
- INPUT SCALAR CONTAINING THE ROW DIMENSION OF
  MATRICES A AND LU IN THE CALLING PROGRAM.
- INPUT OPTION.
  IF IOGI IS GREATER THAN ZERO, THE NON-ZERO
  ELEMENTS OF A ARE ASSUMED TO BE CORRECT TO
  IOGI DECIMAL PLACES. LUDATF PERFORMS AN
  ACCURACY TEST TO DETERMINE IF THE COMPUTED
  DECOMPOSITION IS THE EXACT DECOMPOSITION
  OF A MATRIX WHICH DIFFERS FROM THE GIVEN ONE
  BY LESS THAN ITS UNCERTAINTY.
  IF IOGI IS EQUAL TO ZERO, THE ACCURACY TEST IS
  BYPASSED.
- OUTPUT SCALAR CONTAINING ONE OF THE TWO
  COMPONENTS OF THE DETERMINANT. SEE
  DESCRIPTION OF PARAMETER D2, BELOW.
- OUTPUT SCALAR CONTAINING ONE OF THE
  TWO COMPONENTS OF THE DETERMINANT. THE
  DETERMINANT MAY BE EVALUATED AS (D1)*(D2)
  PERMUTATION INDICES. SEE DOCUMENT
  (ALGORITHM).
- OUTPUT VECTOR OF LENGTH N CONTAINING
  RECIPROCAL OF THE ABSOLUTE VALUES OF
  THE LARGEST (IN ABSOLUTE VALUE) ELEMENT
  IN EACH ROW.
- ACCURACY TEST. PARAMETER, OUTPUT ONLY IF
  IOGI IS GREATER THAN ZERO.
  SEE ELEMENT DOCUMENTATION FOR DETAILS.

```





```

91 EQUIL(1) = ONE/BIG
92 10 CONTINUE
93 DO 105 J=1,N
94 JMI = J-1
95 IF (JMI.LT. 1) GO TO 40
96
97 DO 35 I=1,JMI
98 SUM = LU(I,J)
99 IF (IDGT.EQ. 0) GO TO 25
100
101 C
102
103 C
104
105 C
106
107 C
108
109 C
110
111 C
112
113 C
114
115 C
116
117 C
118
119 C
120
121 C
122
123 C
124
125 C
126
127 C
128
129 C
130
131 C
132
133 C
134
135

```

COMPUTE U(I,J), I=1,....,J-1  
 WITH ACCURACY TEST  
 WITHOUT ACCURACY  
 COMPUTE U(J,J) AND L(1,J), I=J+1,....,

```

105 JMI = J-1
106 IF (JMI.LT. 1) GO TO 40
107
108 DO 35 I=1,JMI
109 SUM = LU(I,J)
110 IF (IDGT.EQ. 0) GO TO 25
111
112 C
113
114 C
115
116 C
117
118 C
119
120 C
121
122 C
123
124 C
125
126 C
127
128 C
129
130 C
131
132 C
133
134
135

```

```

136 45 CONTINUE
137 LU(I,J) = SUM
138 MI = MI + DABS(SUM)
139 IF (AI .EQ. ZERO) AI = BIGA
140 IFEST = MI/AI
141 IF (TEST .GT. WREL) WREL = TEST
142 GO TO 65
143
144 C
145 55 IF (JMI .LT. 1) GO TO 65
146 55 DO 60 K=1,JMI
147 55 SUM = SUM - LU(I,K)*LU(K,J)
148 55 CONTINUE
149 60 LU(I,J) = SUM
150 65 Q = EQUIL(I)*DABS(SUM)
151 65 IF (P .GE. Q) GO TO 70
152 65 P = Q
153 70 IMAX = I
154 70 CONTINUE
155 C
156 70 IF (RN+P .EQ. RN) GO TO 110
157 70 IF (J .EQ. IMAX) GO TO 80
158 70
159 75 D1 = -D1
160 75 DO 75 K=1,N
161 75 P = LU(IMAX,K)
162 75 LU(IMAX,K) = LU(J,K)
163 75 LU(J,K) = P
164 75 CONTINUE
165 EQUIL(IMAX) = EQUIL(J)
166 IPVT(J) = IMAX
167 D1 = D1*LU(J,J)
168 IF (DABS(D1) .LE. ONE) GO TO 90
169 D1 = D1*SIXTH
170 D2 = D2+FOUR
171 GO TO 85
172 IF (DABS(D1) .GE. SIXTH) GO TO 95
173 D1 = D1*SIXTH
174 D2 = D2-FOUR
175 GO TO 90
176 CONTINUE
177 JPI = J+1
178 IF (JPI .GT. N) GO TO 105
179 P = LU(J,J)
180 DO 100 I=JPI,N

```

```

LUDA1440
LUDA1450
LUDA1460
LUDA1480
LUDA1490
LUDA1500
LUDA1510
LUDA1520
LUDA1530
LUDA1540
LUDA1550
LUDA1560
LUDA1570
LUDA1580
LUDA1600
LUDA1610
LUDA1620
LUDA1630
LUDA1640
LUDA1650
LUDA1660
LUDA1670
LUDA1680
LUDA1690
LUDA1700
LUDA1710
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LUDA1730
LUDA1740
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LUDA1760
LUDA1770
LUDA1790
LUDA1800
LUDA1810
LUDA1820
LUDA1840
LUDA1850
LUDA1860
LUDA1870
LUDA1880
LUDA1890
LUDA1900
LUDA1910
LUDA1920

```

TEST FOR ALGORITHMIC SINGULARITY

INTERCHANGE ROWS J AND IMAX

DIVIDE BY PIVOT ELEMENT U(J,J)

AD-A064 545

CINCINNATI UNIV OH DEPT OF ENGINEERING SCIENCE  
A CRITICAL EVALUATION OF COMPUTER SUBROUTINES FOR SOLVING STIFF--ETC(U)  
OCT 78 D C KRINKE, R L HUSTON  
UC-ES-101578-8-0NR

F/G 12/1

N00014-76-C-0139

NL

UNCLASSIFIED

2 OF 2

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A064545



END

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LUDA1930  
LUDA1940  
LUDA1950  
LUDA1960  
LUDA1970  
LUDA1980  
LUDA1990  
LUDA2000  
LUDA2020  
LUDA2030  
LUDA2040  
LUDA2050  
LUDA2060  
LUDA2070  
LUDA2080  
LUDA2090  
LUDA2100  
LUDA2110  
LUDA2120

```

181 LU(I,J) = LU(I,J)/P
182 CONTINUE
183 CONTINUE
184 C
185 IF (IDGT.EQ. 0) GO TO 9005
186 P = 3**I+3
187 WA = P*AKREL
188 IF (WA+10.DO**(-IDGT)) .NE. WA) GO TO 9005
189 IER = 34
190 GO TO 9000
191 C
192 IER = 129
193 D1 = ZERO
194 D2 = ZERO
195 C
196 CONTINUE
197 CALL JER1ST(IER,6HLUDATF)
198 RETURN
199 END

```

PERFORM ACCURACY TEST

ALGORITHMIC SINGULARITY

PRINT ERROR



```

123456789101112131415161718192021222324252627282930313233343536373839404142434445
SUBROUTINE LUELMF (A,B,IPVT,N,IA,X)
C-----D-----LIBRARY 1-----
FUNCTION
USAGE
PARAMETERS A B IPVT N IA X
C-----
-- ELIMINATION PART OF SOLUTION OF AX=B --
-- FULL STORAGE MODE
-- CALL LUELMF (A,B,IPVT,N,IA,X)
-- THE RESULT, LU, COMPUTED IN THE SUBROUTINE
  LU DATA, WHERE L IS A LOWER TRIANGULAR
  MATRIX WITH UNES ON THE MAIN DIAGONAL. U IS
  UPPER TRIANGULAR. L AND U ARE STORED AS A
  SINGLE MATRIX A, AND THE UNIT DIAGONAL OF
  L IS NOT STORED
  B IS A VECTOR OF LENGTH N ON THE RIGHT HAND
  SIDE OF THE EQUATION AX=B
  IPVT - THE PERMUTATION MATRIX RETURNED FROM THE
  SUBROUTINE 'LUDATF', STORED AS AN N LENGTH
  VECTOR
  N - ORDER OF A AND NUMBER OF ROWS IN B
  IA - NUMBER OF ROWS IN THE DIMENSION STATEMENT
  X - FOR A IN THE CALLING PROGRAM,
  THE RESULT X
  - SINGLE/DOUBLE
  - FORTRAN
PRECISION
LANGUAGE
LATEST REVISION - APRIL 11, 1975
C-----
DIMENSION A(IA,N),B(N),IPVT(N),X(N)
A,B,X,SUM SOLVE LY = B FOR Y
DO 5 I=1,N
  X(I) = B(I)
  IW = 0
  DO 20 J=1,N
    IP = IPVT(I)
    SUM = X(IP)
    IF (IW.EQ. 0) GO TO 15
    IM1 = I-1
    DO 10 J=IW,IM1
      SUM = SUM-A(I,J)*X(J)
    CONTINUE
    GO TO 20
  10 IF (SUM.NE. 0.) IW = I
  15

```

LUEF0470  
 LUEF0480  
 LUEF0490  
 LUEF0500  
 LUEF0510  
 LUEF0520  
 LUEF0530  
 LUEF0540  
 LUEF0550  
 LUEF0560  
 LUEF0570  
 LUEF0580  
 LUEF0590

SOLVE JX = Y FOR X

```

46 C
47 20 X(I) = SUM
48 DO 30 IB=1,N
49 IPI = N+1-IB
50 IPI = I+1
51 SUM = X(I)
52 IF (IPI:GT,N) GO TO 30
53 DO 25 J=IPI,N
54 SUM = SUM-A(I,J)*X(J)
55 CONTINUE
56 X(I) = SUM/A(I,I)
57 RETURN
58 END
59

```



UERT0470  
 UERT0480  
 UERT0490  
 UERT0500  
 UERT0510  
 UERT0520  
 UERT0530

```

46 20 IER2=IER2-IBIT(IER1)
47 C
48 WRITE (PRINT,25) (ITYP(I,IER1),I=1,5),NAME,IER2,IER
49 25 FORMAT('*** 1 M $ L(UERTIST) ***',5A4,4X,3A2,4X,12,
50 * (IER = ',13,')')
51 RETURN
52 END
  
```

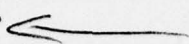
PRINT ERROR MESSAGE



(9) Technical rept. 2 Sep 77-  
15 Oct 78

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number)  A number of commonly available computer subroutines for solving differential equation systems are tested and compared for their ability to solve "stiff" systems.  A "stiff" system is defined as either: 1) a system with widely separated eigenvalues or time constants or 2) a system with diverging exponential terms which have small or zero coefficients due to a particular		

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choice of initial conditions. For example, it is believed that the governing differential equations of large complex mechanical system models (such as, human-body/crash-victim simulation models, finite segment structural models, and large vibrating system models) are frequently stiff. 

The solver subroutines tested on such systems are as follows:

- 1) DRKGS (a fourth-order Runge-Kutta routine); 2) DHPCG (a Hamming predictor-corrector routine); 3) DVOGER-ADAMS (an Adams predictor-corrector routine); 4) DVOGER-GEAR (a Gear predictor-corrector routine) 5) DREBS (a Bulirsch-Stoer routine); and 6) RK45 (a sixth-order Runge-Kutta routine).

These solver subroutines are tested and compared for a number of stiff systems of both types described above where the exact analytical solution is known. The subroutines are compared in terms of run time, accuracy, and function calls. It is found that the subroutines vary considerably in terms of accuracy. Also, their overall individual effectiveness is highly dependent upon the specific system being solved. However, for systems of the first type of stiffness, Gear's method (DVOGER-GEAR) and DRKGS appear to be the preferred routines. Finally, the automatic stepsize capability of DRKGS and DHPCG is a definite advantage over the other routines. However, the step oriented format of DVOGER and DREBS provides a potential for similar flexibility in error control through coding modifications.